

**DESIGN AND DEVELOPMENT OF A MICROCAVITY HOLLOW  
CATHODE GLOW DISCHARGE EMISSION SYSTEM FOR  
SIMULTANEOUS MULTIELEMENT ANALYSIS OF DISCRETE  
HANGING PLATE SOLUTION RESIDUES**

BY

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To Will, Dale and Dorothy - thanks for keeping my spirits up

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CATHODE GLOW DISCHARGE EMISSION IONIZATION FOR  
SIMULTANEOUS MULTIELEMENT ANALYSIS OF DISCRETE  
HANDSAMPLES OF SOLUTION RESIDUES**

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The hollow cathode glow discharge is a rather modest atomic emission source, but, nevertheless has many desirable characteristics. The discharge is easy to initiate and sustain, providing sharp atomic lines with a low background continuum. The low pressure environment readily eliminates chemical reactions, matrix effects and self-absorption. The scattered spectrum association process yields an atomized representation of the bulk material.

Although theoretically the hollow cathode glow discharge is nearly wavelength neutral, in reality it has different than weak signal output. It has been shown that cathode geometry plays an important role in the signal emission signal intensity.

The hollow cathode geometry increases the ionization probability over the planar cathode, but are enough to rival other atomic emission sources. The work presented in this dissertation focuses on the use of a microarray hollow cathode glow discharge (MCHGDD) as a method to enhance signal output.

Although there are several effective multielement techniques at use today, they all require large sample volumes. There are circumstances, however, in which only a very small sample may be available (e.g. forensic samples and precious bodily fluids) but the determination of many elements on the trace and ultra-trace level may be required. This project investigates the applicability of MCHGDD to the simultaneous multielement analysis of discrete microsamples of solution residues.

Several important diagnostic parameters were determined, including pressure, voltage, current, sample drying time, air width and chamber porosity.

The experimental investigation was performed in two phases. The first phase evaluated the MCHGDD emission system as a source for ultratrace analysis. Single element analysis of Cu and Pb was performed using each element's strongest emission line. The limits of detection, 3 pg for Cu and 36 pg for Pb, demonstrated that the MCHGDD is an excellent source for ultratrace analysis. The second phase evaluated the MCHGDD emission system as a multielement source. Simultaneous determination of Pb, V, and Cr was achieved, demonstrating that the MCHGDD is a good multielement source.

## CHAPTER 1 INTRODUCTION

### Character of the Glow Discharge

The glow discharge is a rather modest open plasma which is generated upon spark breakdown between two electrodes immersed in a low pressure, rare gas environment. It is a self-maintaining discharge easily extinguishable under a certain set of conditions: pressures ranging from 1-10 Torr, applied voltage ranging from 400-2000 V and currents ranging from 1-1000 mA, depending on the rare gas-electrode material combination.

In that low pressure environment, the glow discharge is visually free from self-disruption and will extend  $1^{\circ}$  to yield narrow spectral bands<sup>1</sup> and provide an even cloud representation of the bulk material being sampled<sup>2</sup> with sizes decreasing ranging from  $10^7 - 10^{10}$  cm<sup>-3</sup>.<sup>3</sup>

The ground state free atom population, necessary for atomic emission spectra, is generated by a nonthermal ionization scattering process. Because the scattering process is non thermal, many of the interferences associated with thermally excited sources, such as noise effects and sample vaporization, are not associated with the glow glow discharge. The subsequent excitation of the free particles scattered from the solid matrix occurs as a result of the energy generated

in an electric field. Consequently, the glow discharge falls into the category of arcless discharges. The categories of plasma sources covered are presented in Table 1-1.

Table 1-1 Categories of Plasma Discharge Sources.

#### Thermal Sources

##### High Temperature Sources Plasmas

#### Electron Discharge Sources

##### Low Pressure:

- AC
- Glow Discharges
- Flame Catheric
- Hollow Cathode
- Gunster Discharges

##### Atmospheric Pressure

- AC
- DC Arcs
- High Voltage n.c. Arcs
- Sparks
- Plasmas
- Bipolar Arcs
- Acetone/Hydrogen
- Plasmarons
- RF Discharges
- Inductive
- Capacitive
- Microwave Discharges
- Capacitive
- Microstrip Induced

through the glow discharge is a major advantage, both in electrical energy<sup>1</sup> of gas, been shown to be an effective radiation source and the fact that it is easily coupled to a wide variety of detection systems, for use in atomic absorption,<sup>1,2</sup> atomic fluorescence,<sup>3,4</sup> atomic emission,<sup>5,6</sup> resonance ionization<sup>7</sup> and mass spectrometry.<sup>8,9</sup> Applications for the glow discharge source have been extensive and include analysis of metal alloys,<sup>10-12</sup> determination of gases in metals,<sup>13</sup> determination of trace metals in biological tissues,<sup>14</sup> analyses of solution residues<sup>15-17</sup> and property analyses of thin films and semiconductors.<sup>18-21</sup>

One of the reasons for the wide applicability of the glow discharge is the broad range of excitation energies achievable with the use of different noble gases. Table 1.2 lists the energies of the long-lived triplet metastable levels characteristic of all the noble gases. These triplet states are associated with the excitation of the analytic species.<sup>22</sup> Any element with an oxidation potential at or below the excitation potential of the noble gas is able to be sufficiently excited by the noble gas. Nearly all of the elements are excitable by one or more of the noble gases.

Table 1.2 Excitation Potentials of the Noble Gases<sup>22</sup>

Noble Gas	Excitation Threshold (eV)
Helium	20.55, 19.77
Argon	17.45, 11.86
Potassium	16.62, 14.72
Krypton	9.86, 10.31
Xenon	8.28, 9.40

## Historical Developments

The glow discharge is an old analytical tool. On the contrary, it has been widely investigated since 1891 when Friedrich Paschen first explored its potential as a spectral source. Paschen induced a Gouy tube with an evacuated glass-tube hollow cylinder to serve as the cathode. Upon evacuation of the tube below 1 Torr, and with a sufficient applied voltage, he observed a glow wholly contained within the hollow cylinder. He varied the pressure and current density until a stable discharge was achieved and recorded the emission spectrum of helium. Paschen is credited with the first application of the glow discharge source to spectroscopic analysis.<sup>1,2</sup>

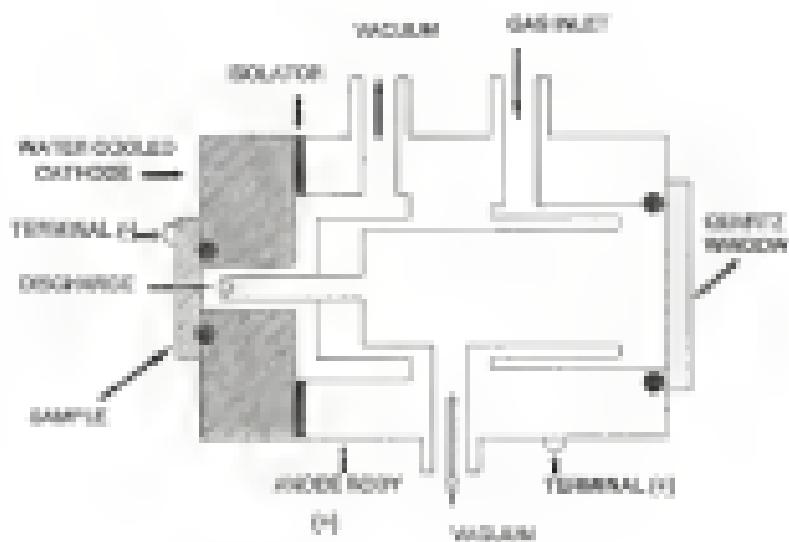
Since Paschen's groundbreaking work, the glow discharge has enjoyed a steady, albeit sporadic, evolution. In 1928, Tolokhov<sup>3</sup> reported on his early studies of the excitation processes in the hollow cathode glow discharge source. Sawyer<sup>4</sup> added to the knowledge of glow discharges with his studies on cathode materials and source gases. Tolokhov's research<sup>3</sup> in the late 1920's focused on the quantized spectra analysis of hydrogen structures as well as the influence of the hollow cathode glow discharge for analyzing small samples.<sup>12</sup> After a 15-year period of passivity in glow discharge research, McNally<sup>5</sup> published the results of quantitative studies on cathode materials. This was the first work that proved a direct relationship between signal intensity and the amount of apportioned material. McNally's results spurred a renewed interest in the glow discharge and led to a

period of atomic spectrograph of the glow discharge throughout the 1970s and 1980s.

In the 1980s, the research primarily focused on using the hollow cathode glow discharge technique as a source for atomic absorption studies.<sup>21</sup> In the 1990s, the Russians investigated the hollow cathode glow discharge as an atomic emission source<sup>22</sup> while Wastford<sup>23</sup> paved the way for glow discharge excited fluorescence. In 1993, Gross<sup>24</sup> introduced a glow discharge source which combined the best characteristics of plasma and hollow cathode discharges. The Gross glow discharge source extended the applicability of glow discharge spectrometry to a wide variety of solid conducting samples as well as non-conducting powders.<sup>25</sup> A typical Gross type glow discharge is illustrated in Figure 1-1 (from Human<sup>26</sup>).

The 1990s was a decade of growing interest in glow discharge research. The source had proved highly suitable for atomic absorption spectroscopy but was disappointingly inadequate as an atomic emission source. More robust and powerful atomic emission sources, like the extensively improved plasma, were capturing the interest of research groups around the world. Problems with designing demonstrators hollow cathode for novel sample analysis were the major stumbling blocks to further development of the glow discharge source. There were also problems with contamination of the carrier gas by air and water vapor as well as difficulty maintaining oxygen saturation requirements.

Figure 4-1 Schematic cross section of a Grimm-type glow discharge



Interest was again sparked in the 1970s as researchers turned their attention back to investigating the hollow cathode discharge as a spectral source. Up until this time, the advantages of the glow discharge, i.e. high emission efficiency, high stability, low background intensity, narrow spectral linewidths, low cost and absence of moving interferences and thermal effects, had investigations to believe the glow discharge might prove to be an ideal source. In actual performance, it was disappointing because the major disadvantage found in working with the hollow cathode glow discharge was its comparatively weak signal output. Research over the past decade has focused on improving the source by increasing the discharges with the expectation that it could be used for trace and ultra-trace analysis.

#### Recent Developments in Hollow Cathode Glow Discharge Ionization

As previously stated, recent modifications of the hollow cathode glow discharge ionization have been aimed at enhancing the analytical signal output.

The signal boosting technique that has been very successful has been to couple the glow discharge to another form of external energy. Caneiro<sup>17-19</sup> has successfully coupled the hollow cathode glow discharge with a 2000 MHz microwave generator. There are basically two electron populations in the glow discharge - fast electrons responsible for collisional excitation and the last energetic slow electrons responsible for ionization processes. Coupling the two microwave sources, the microwave plasma and the glow discharge, results in a

higher density of fast electrons, which, in turn, increases ionization of noble gas, as well as the density of metastable species. The increase in noble gas gas atoms eventually leads to an increase in noble ionization through Penning ionization processes. The analytical signal is enhanced by at least an order of magnitude while the intensity of the background spectrum of the noble gas is lowered. Krueger<sup>22</sup> and Becker<sup>23,24</sup> both applied an external magnetic field to the hollow cathode glow discharge. It was found that the magnetic field did not affect the motion of the atoms and ions, the electron density, the ionization cross sections of the atoms, the mean free path of the electrons, the spontaneous radiance, the background emission or the quenching collisions. It did, however, affect the motion of the charged particles in the plasma, causing the high energy beam electrons to migrate to the chamber walls, allowing the low energy electrons, responsible for the ionization processes, to predominate. It was determined that with an increase of the external magnetic field, the analytical signal, as well as the discharge current, showed an increase while the noble gas line intensities remained unchanged. Decreases in limits of detection using this technique range from 1-3 orders of magnitude.

Another ionizing technique that has enjoyed a great deal of interest is the RF-excited pulsed hollow cathode glow discharge. In this technique, a current pulse is applied to the anode followed by a short burst of rf energy. The sinusoidal product produced by the current pulse is subsequently recorded by the rf burst

Arai<sup>23</sup> and Pustovik<sup>24</sup> had good success with this technique, reporting a 3 times signal enhancement when comparing the effluent versus the carrier pulse.

Beam cathode geometry has been shown to have a significant effect upon signal output.<sup>25</sup> boosting techniques which alter the cathode geometry have also been investigated, the most important of which is the use of a monocavity hollow cathode. The monocavity hollow cathode refers to hollows of less than 2 mm in diameter. Nevelsides and Tammes<sup>26</sup> developed an empirical formula to express the relationship between the spectral line intensity ( $I_0$ ) and the cathode diameter ( $D$ )

$$I_0 = k \quad (6)$$

where  $k$  is a constant. Experimental data has confirmed that the smaller the diameter of the hollow, the greater the spectral line intensity. The length-to-diameter ratio of at least 0.1. Several phenomena are responsible for the two order of magnitude decrease in diameter hohlraum using this cathode.<sup>27</sup> The small cavity size decreases the electron energy allowing the low energy excitation process to dominate. There is also an increase in the concentration of the excited species, an increase in the current density and an increase in the residence time of the analyte. Any one of these phenomena would certainly increase the intensity of the atomic signal, together they have a synergistic effect. The monocavity hollow cathode glow discharge is the focus of the work detailed in the Discussion.

## Scope of Dissertation

There are several effective analytical techniques at use today which allow for simultaneous multielement analysis, including inductively coupled plasma atomic emission spectroscopy, inductively coupled plasma mass spectrometry, microwave plasma techniques and flame-emission. As effective as these methods may be, they all require large sample volumes. There are circumstances, however, in which a multielement analysis on the trace or ultratrace level is required but only a small sample is available for the analysis, e.g. forensic samples and previous bodily fluids. The need for a technique which can analyse discrete microliter/hundred microliter samples for many elements simultaneously is evident. The development of this necessarily hollow cathode glow discharge emission system is in response to this need.

The first chapter of this dissertation will introduce the glow discharge as an analytical source and present an overview of the historical background of the hollow cathode glow discharge. Recent developments in signal enhancement techniques will also be discussed. An in-depth discussion of the fundamental processes that occur in the glow discharge will be presented in chapter 2. In chapter 3, the details of the design and development of a microanalytical hollow cathode glow discharge emission system will be highlighted. Chapter 4 will focus on two series of experiments involving single element determination of copper and lead in complex metal solution matrices using the microsystem. The results

presented in this chapter will support the contention that the microconical hollow cathode glow discharge is an excellent source for ultimate analysis. Chapter 5 will highlight a series of experiments designed to analyze nuclear waste samples for more than one element at a time. The results presented in this chapter will support the contention that the microconical hollow cathode glow discharge is an excellent multielement source. Chapter 6 will put together the results from chapters 3-5 and will make the case that the microconical hollow cathode glow discharge atomic system shows great potential as a valid multielement technique for diverse nuclear samples. Future work and improvements to the system will also be discussed.

## CHAPTER 2. LOW PRESSURE DISCHARGES

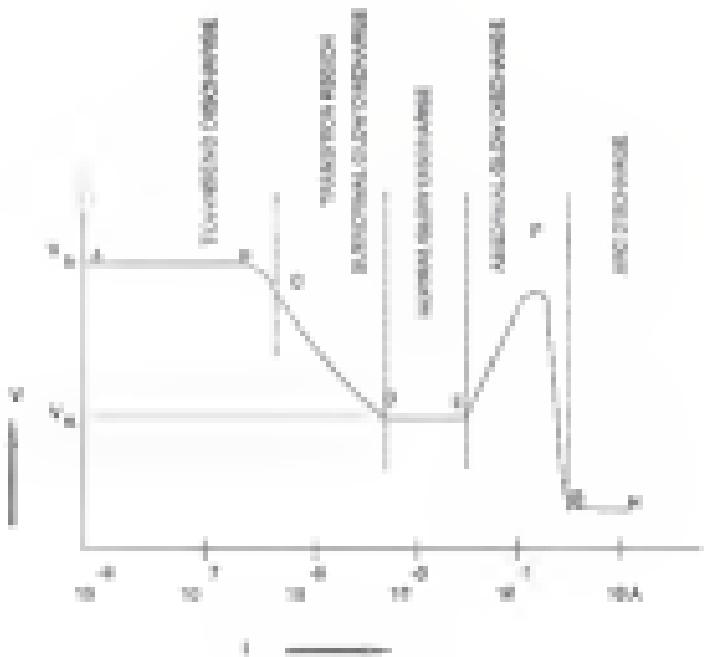
### Resistive Discharges and Characteristics

#### Type of Low Pressure Discharges

There are several types of gas discharge that can be generated between two electrodes at a low pressure rare gas environment. Figure 2.1 plots the voltage-current characteristics of four of them.

The first type of discharge, the Townsend discharge, is described by equation A6 in Figure 2.1, and is a dark, non self-sustaining discharge. The voltage that is applied to the cathode creates an electric field between the electrodes. Electrons emitted by the cathode migrate toward the anode. In traversing the distance between the cathode and anode, a number of electron impact ionization collisions occur with the rare gas atoms. The positive ions thus created are swept toward the negatively charged cathode. In a Townsend discharge, there is a steady-state relationship between newly created ions and the discharge current. The number of ions arriving at the cathode is exactly equal to the number of electrons impinging on the anode. Since this type of discharge is entirely dependent upon an external initiation source (the applied voltage to the cathode) and, in fact, extinguishes immediately upon its removal, the Townsend discharge is not a self-

Figure 3.1 Voltage current characteristics of low pressure discharge<sup>12</sup>



vacuum discharge. This type of discharge can only be generated at very low currents where the positive ion space-charge distortion of the field is relatively small.<sup>13</sup>

In the second section of figure 2-1, CD, it is clear that with an increase in current of the same pressure comes a change in the voltage. As the current reaches the discharge conditions, there is an instant in time to reach the discharge. The voltage required to sustain the discharge subsequently decreases as the number of electrons which carry the current increases. At this point, there is an onset of what is called an electron avalanche and electron multiplication begins to take place. The voltage-current characteristics of region CD do not describe a type of discharge but rather a transition region between the dark one self-sustaining discharge to a luminescent discharging discharge.

The next type of low pressure discharge depicted in figure 2-1 begins at point D, where, with an increase in current, the normal cathode fall potential,  $V_{nk}$ , is reached and a visible glow is observed. This type of discharge is called a "normal glow discharge". The current is now sufficient for main electron multiplication to occur. Under these conditions, a self-sustaining luminescent discharge, not solely dependent upon an external cathode heater source, is generated. This means that each electron emitted by the cathode causes secondary potentials to exist in the active region of the discharge, which result in the original electron being replaced by a newly emitted electron from the cathode. In this "normal"

"glow discharge" regime. The cathode (A) potential is maintained at 200-300 V and remains constant even with large increases in current, from 10<sup>4</sup> to 8.1 A.

Upon additional increases in current, the current density physically expands across the cathode surface until the surface is saturated. At this point, it in Figure 2-1, any increase in current results in an increase in voltage. This kind of discharge is referred to as an "observed glow discharge" and is the type of low pressure discharge most often used in glow discharge work.

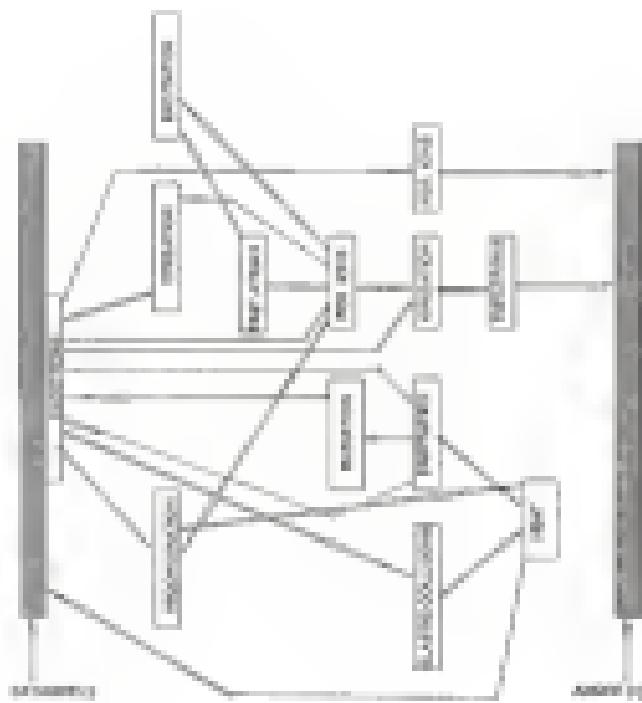
The last type of low pressure discharge represented in Figure 2-1 is the arc discharge. As can be seen in region PGM, an increase in current results in a sudden drop in voltage to only tens of volts. The arc discharge is characterized by high current and low voltage. Electron emission from the cathode is primarily the result of thermionic emission, as opposed to the other low pressure discharges, where electron emission occurs as a result of a cathodic sputtering.

#### Features of the Arc and Glow Discharge

The observed glow discharge, hereafter referred to simply as the glow discharge, is generated by passing an acclimating current through a rare gas under low pressure. The elementary processes which occur in the glow discharge as a result of the electrical discharge are numerous and complex. Figure 2-2 summarizes the various processes which are summarized in Figure 2-2.

Visually, the glow discharge has a distinct structure of alternating zones of varying luminosity.<sup>17</sup> These zones are best understood by analyzing the creation

Figure 3-2 Schematic diagram of chemistry processes in a glow discharge.<sup>18</sup>



of a glow discharge governed between two plane parallel electrodes, as depicted in Figure 3(b). Each zone represents an area of the discharge undergoing characteristic physical processes, i.e. excitation and ionization.<sup>10</sup>

Closer to the cathode is a thin layer called the Anode dark space. Low energy electrons emitted by the cathode via secondary emission begin their journey to the anode in this space. Catherod<sup>11,12</sup> has recently modeled the Anode dark space and has suggested that the electrons are emitted from the cathode with a range of energies from 0 to 14 eV. Although the electrons maintain this range of energies throughout most of the Anode dark space, they begin to pick up energy and momentum as they are repelled from the negatively charged cathode.

In the adjacent cathode glow region, the electrons have gained enough energy to cause some collisional excitation of the rare gas atoms. A very weak glow is observed in this region. The cathode glow is also a very small region of the glow discharge. Its thickness is dependent upon the type of rare gas and the gas pressure.<sup>13</sup>

Since the glow discharge is a self-sustaining discharge and the electrons necessary to sustain the glow come from interactions between the cathode material and the rare gas rather than from the anode anodes, there must be a region in the discharge where ionization of the rare gas atoms and electron multiplication take place. This region is known, variously, as the cathode dark space, Crocker's dark space or Filmer's dark space. The cathode dark space follows the cathode

**Figure 1.3** Representation of the main features of a planar glow discharge



glow region and represents the point where the electrons are so energetic they move collisionless whenever rather than collisional otherwise. The cathode dark space occurs since the outer cathode fall potential of the discharge<sup>21</sup> through an initially high and then linearly decreasing electric field.<sup>22</sup> This covers the positive ions in motion toward the negatively charged cathode and the electrons to be ejected over the next region of the discharge, the negative glow. This is an ionizing process and since the electron mobility is so much greater than the ion mobility, the cathode dark space is a region of high positive ion density.<sup>23</sup> Toward the cathode end of the cathode dark space, the charge density increases.<sup>24</sup> Overall, the cathode dark space is the most important zone of the glow discharge and is essential for maintaining the current flow.<sup>25</sup>

In a planar cathodic glow discharge, there are two distinct populations of electrons which emerge from the cathode dark space and enter the negative glow. These electrons which have accelerated across the cathode drop without undergoing Coulomb collisions near the negative glow with energies upwards of 100 eV.<sup>26</sup> These fast beam electrons are responsible for the ionization processes at the very beginning of the negative glow region. They penetrate only a short distance, 1-2 mm,<sup>27</sup> before they lose their energy, mainly through Coulomb collisions with rare gas atoms. The second population of electrons are the slow plasma electrons with energies ranging from 0.1 to 20 eV. These electrons come from the anode. A small number of electrons emitted from the cathode, which

have undergone ionization collisions before reaching the negative glow, enter the region with energies ranging from 0.1 to 1 eV.<sup>10</sup> The great majority of plasma electrons come from ionization processes within the first one-half of this region, so the beam electrons are ejected into the negative glow. The range of energies of these plasma electrons is from 10 to 20 eV.<sup>10</sup> The plasma electrons are responsible for the excitation processes that occur in the negative glow. Since they are, by far, the most abundant type of electron in the zone, the negative glow is the most luminous region of the entire discharge. The great majority of the slow plasma electrons have sufficient energy to cause excitation of the rare-gas atoms and ions as well as resonance transitions of most of the elements. Clearly, this is the region of interest for spectral analysis.

The negative glow is actually a neutral plasma with either high-,  $10^9$  to  $10^{10}$   $\text{cm}^{-3}$ , but approximately equal concentrations of positive ions and electrons. The ground-state argon atom population figure has been shown to be on the order of  $10^3$  to  $10^4$   $\text{cm}^{-3}$  using the net ionization degree somewhat less than 10%.<sup>10</sup> The ground-state argon atom population has been measured at values from  $10^9$  to  $30^9$   $\text{cm}^{-3}$ .<sup>11,12</sup>

The electric field in the negative glow is very low and nearly uniform throughout. This very low field gradient is the characteristic of a "nearly nonconductive" plasma region.

Physical studies of the negative glow have yielded good information about the diffusion processes that govern the plasma region. One important measurement is determining the diffusion processes present in a discharge or the Debye length. This varies as the square root of the ratio of the electron temperature to the electron density<sup>12</sup>. In the negative glow, the electron temperature as well as the electric field is low<sup>13,14</sup> compared to a cathode leap electron density,  $10^9$  to  $10^{11}$  cm<sup>-3</sup>, thus making the Debye length very small. When the Debye length is small compared to the dimensions of the glow discharge chamber, radial diffusion losses of charged particles are governed by unipolar diffusion<sup>15</sup>. This theory holds true for the negative glow region.

Inwardly following the negative glow is the Faraday dark space (FDS). This region is characterized by a slight rise in field as the electron population decreases and additional voltage is needed to sustain the current flow. The FDS is composed of ground state particles and low energy electrons which lose their energy in the immediately outer negative glow region. This region is a transition region between two plasma zones, the negative glow and the positive column. The boundaries of the FDS are not clearly defined but blend into the adjacent plasmas.

Studies of the FDS show it to be a region of decreasing electron density from the high densities in the negative glow to the low densities in the positive column. The field as well as the electron temperature increase toward the positive

column. The Debye length is on the order of  $1\text{E}^{-5}$  cm making this a quasineutral region not governed by unipolar diffusion theory.<sup>22</sup> The flow of current is dictated by drift flow in the field gradient.

Having gained enough energy ( $20\text{ eV}$ )<sup>23</sup> in the preceding PDS field, the electrons are accelerated toward the anode producing the luminescent positive column along the way. As previously noted, the positive column is the second plasma region in the glow discharge. It is much less luminous than the negative glow, but can be much larger in size depending upon the separation between the cathode and the anode. The length of the cathode region (anion dark space, cathode glow, cathode dark space and negative glow) is dependent upon the type and the pressure of the rare gas at a given voltage. On the other hand, the length of the positive column and the PDS are determined by the separation between the electrodes. If a glow discharge is generated in a long tube, such as a neon light, the positive column in the glow tube is observed throughout most of its length. However, since neither the PDS nor the positive column are usually necessary to produce or maintain the glow discharge, they can be easily eliminated by placing the anode at the end of the negative glow region. This produces an elongated glow discharge and is the basis for the so-called Geen type glow discharge. The minimum separation between the electrodes for the formation of a stable discharge is about twice the thickness of the cathode dark space.<sup>24</sup>

The positive column is characterized by a low voltage gradient and a reduced electron density,  $10^8 \text{ cm}^{-3}$ . A typical representation of the calculation from the positive column shows electrons resulting from low energy atom ionization with silicon as emission from ions. Most of the energy loss in the negative space at the walls of the chamber due to multipolar effects of  $\log^{-1}$ . Comparatively little energy is lost to radiation.

The next region of the glow discharge consists of an anode dark space and an anode glow region. As electrons emerge from the positive column and stream toward the anode, they are relatively low enough in energy that they are unable to excite the neutral gas atoms in the area. There is shown no glow in this region, thus the name anode dark space. The electrons do, however, pick up enough energy for excitation as they accelerate toward the anode and a glow region can be observed immediately adjacent to the anode.

#### Characteristics of the Abnormal Glow Discharge

With the fundamental work of Paschen, Beuyer, Schlier, McNally and others, the glow discharge was long ago proven to be a good spectroscopic source. Since that time, it has been extensively studied and very well characterized, as discussed in Figure 2-4.

As can be seen in Figure 2-4 (L), evolution from the glow discharge to more intense in the two plasma regions, the negative glow and the positive column. Every region in the discharge is, however, bounded to some extent. The dark

which only appear continuous or diffuse in the brightly glowing regions. The negative glow is the region of greatest current with maximum heat dissipation from both acoustic and wave processes.

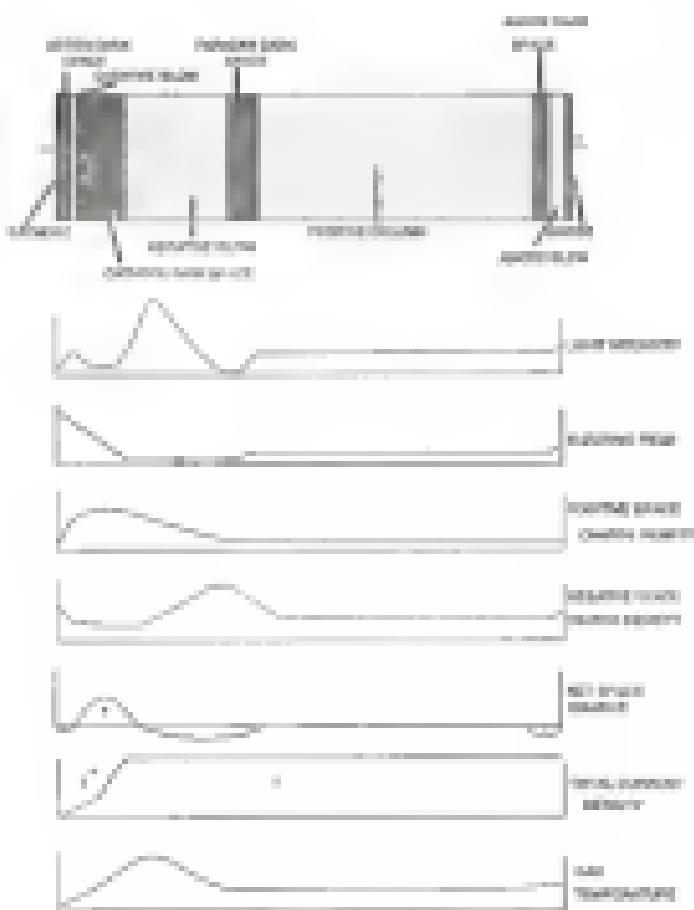
The distribution of the electric field in the glow discharge is very interesting. Figure 2-4 (f) shows the major fields, which are confined to areas close to the electrodes, as well as a neutral field throughout the plasma regions of the discharge. There are two observed field reversals.<sup>22</sup> The first one occurs close to the negative glow region where the field decreases as the electron density gradient increases. In this region, no electric field is needed to carry the total current. Antipolar diffusion except the electrons along mostly and the positive ions mainly. The second field reversal occurs in the Faraday dark space where there is a dissociation of the electron population due to radial diffusion forces. Here, an increase in the field is necessary to maintain the current flow.

The positive, negative and net space charges, illustrated in figures 2-4 (c), (d), and (e), correspond to the physical processes occurring in the various regions as described in the previous section.

The current density is illustrated in figure 2-4 (f) showing regions of ion ( $I^+$ ) current and electronic ( $e^-$ ) current.

Another aspect of interest is the distribution of gas temperature throughout the discharge, as shown in Figure 2-8 (g). A plot of the temperature vs. distance from the cathode shows the area where entropy is lost in heating of the gas. The

Figure 2-4. Characteristics of a plasma glow discharge.<sup>12,13</sup>



gas temperature in the negative glow is approximately 1000 K<sup>12</sup> and in the positive column approximately 300 K.

### Cathodic Sputtering

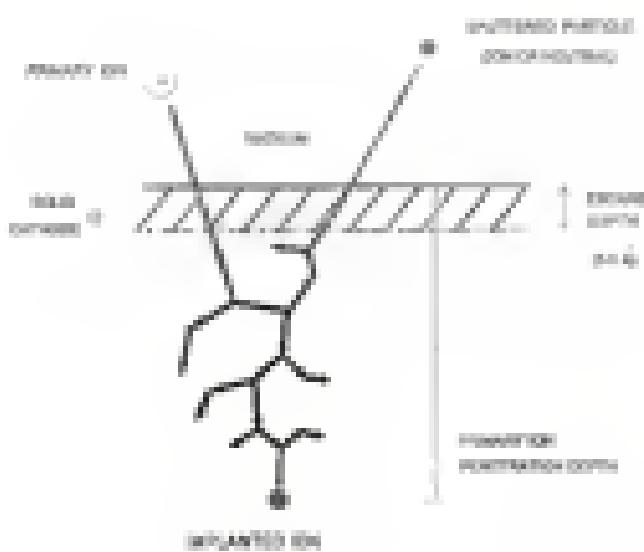
One of the most important advantages of using the glow discharge as a sputtered source is its nonthermal sputtering ionization process.

In a low pressure environment, the negatively charged cathode is subjected to severe positive ion bombardment. A transfer of momentum takes place between the incident ion and a matrix particle (a neutral atom, ion, cluster or electron) through a collisional cascade.<sup>13-15</sup> If a sufficient amount of energy is transferred to the target atom to overcome the matrix-particle binding energy, a surface particle will be ejected. Figure 2.5 illustrates the sputtering process. Over 90% of the sputtered particles are ground state neutral atoms. A few percent are ions and a small fraction may be clustered particles.<sup>16</sup>

Because sputtering is essentially a nonthermal process, thermal evaporation of the sample contributes <0.1% to the primary source of surface particles.<sup>17</sup>

Sputtering efficiency or sputtering yield, is a measure of the number of sputtered particles per incident ion. It is dependent upon the energy of the impacting ion as well as the ion-gas-analyte combination. The energy of the impacting ion is determined by the external applied voltage. The higher the voltage, the higher the cathode fall potential and the more energetic the ion. The total discharge potential is not solely comprised of the cathode fall potential.

Figure 3.9 Schematic representation of the sputtering process.



There is a small plasma potential associated with the secondary electrons in the discharge. It is, however, negligible (1-4 V) compared to the external applied voltage (1000-3000 V) and can be neglected.<sup>12</sup> The ion energy can be considered equal to the applied voltage.

Studies have shown that the impacting ion must have a minimum threshold energy of between 15 and 25 eV in order to effuse atoms of a target metal.<sup>13-15</sup> The sputtering yield then increases linearly up to sputtering energies on the order of 100 eV. The yield then levels off and decreases at very high impact energies (1 keV)<sup>16</sup> at which point, the incident ion penetrates too deeply into the metal and no sputtering takes place.<sup>17</sup> The sputtering yield is also affected by the mass of the analysis atom and the incident ion. The yield has been found to increase with increasing mass of the impacting ion achieving a maximum yield when the masses of the impacting ion and the target atom are the same.<sup>18</sup>

The sputtering yield in atoms per incident ion,  $S$ , can be determined by considering the energy,  $E$ , and mass dependence of the incident ion,  $m_i$ , and target atom,  $m_t$ , system:<sup>19</sup>

$$S = \frac{3\pi}{8\pi} \frac{\sin(\theta/2)}{(m_i/m_t)^{1/2}} \frac{E}{U_s} \quad (2)$$

In this expression,  $U_s$  represents the surface binding energy (eV),  $E$  is the energy of the incident ion (eV),  $\theta$  is a monotonic increasing function of the ratio  $m_i/m_t$  and equal to 0.17 if the ratio is 0.1 and increasing to 1.4 for  $m_i/m_t = 10$ .

Equation 1 predicts a linear relationship between the sputtering yield and the energy of the incident ion and holds true for pure metals and mixtures; ion energies up to 1 keV. It also predicts an inverse relationship between the sputtering yield and the surface binding energy or adhesion energy.

### Cathode Geometries

#### Hollow Cathode

The dimension of the cathode and characteristics of the glow discharge that for pointed apertures to glow discharges produced between planar cathodes. Studies have shown that by altering the geometry of the cathode from a planar configuration to a hollow cylinder, the emission intensity increases by 2-3 orders of magnitude<sup>10-11</sup>. This "hollow cathode effect" is wholly a result of the altered geometry of the cathode. The areas regions and characteristics of the planar cathode glow discharge occur in the hollow cathode glow discharge but they are arranged differently. The regions necessary for the production and maintenance of the discharge, namely the cathode sheath and negative glow, are confined within the hollow, while the anode regions (the FDD, the positive column, the anode dark space and the anode glow) are confined to the cavity.

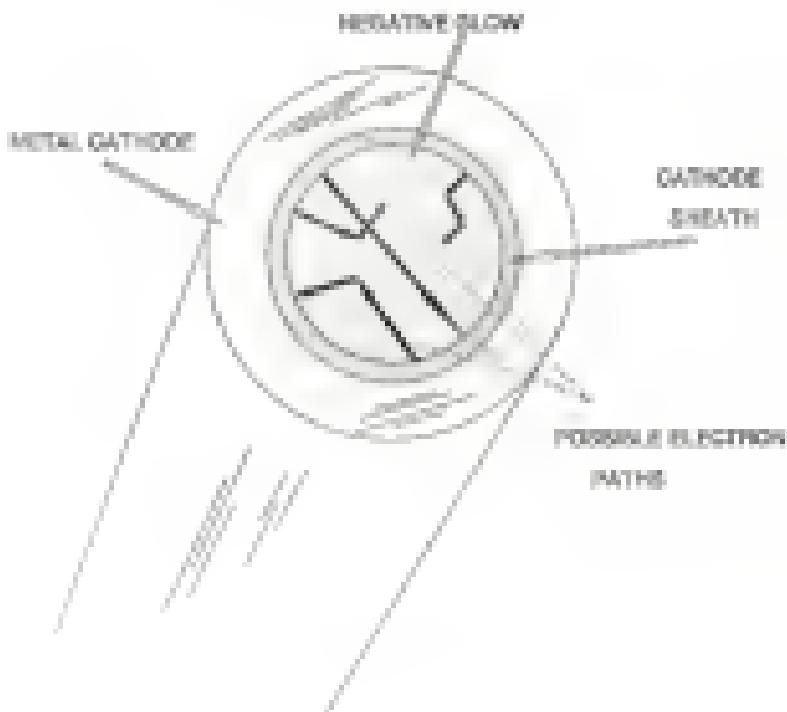
To illustrate how this type of discharge develops, a study was performed which replaced the single planar cathode with a U-shaped cathode, the opening of which faced the anode.<sup>1</sup> The discharge currents were measured as a function of the separation of the side arms of the U-shaped cathode. In effect, it was the

placing two flat cathode discharges parallel to each other, reducing the separation between them and then observing the resulting discharge. At an initial separation of 25 mm, the discharge appeared to be two distinct discharges separated by a dark space in the center. The emission intensity was comparable to a discharge with a single planar cathode. When the separation between the arms of the U-shaped cathode was decreased to 8 mm or less, the two negative glow regions were observed to coalesce into a single much brighter discharge. Overlapping the negative glow regions had a dramatic effect on the emission intensity. Measurements of emission line intensities showed a 200- to 1000-fold increase in the  $\lambda_1$  peak.

The geometrical configuration must modify and re-achieve the hollow cathode effect in the hollow cylinder, with one or both ends open. The cathode layers which are observed in the planar glow discharge are also present in the vicinity of the hollow cathode, but are arranged in a circular manner as shown in Figure 3-6.

Electrons emitted from the cathode cover a narrow, 0.81-0.87 mm,<sup>10</sup> cathode-anode region (Anode-dark space, cathode glow, and cathode-dark space). Because of some of the physical processes that occur in the hollow cathode glow discharge, this cathode-anode region is much smaller than the similar region of a planar glow discharge. The electrical characteristics, however, are the same. The electric field is initially very high and decreases linearly with distance from the

Figure 2.6. Representation of a hollow cathode glow discharge



cathode surface to near zero at the negative glow region. The cathode-dark space region around the entire cathode has potential at a dose with a planar cathode. However, since it has to carry the potential through a much smaller distance, the field gradient is much steeper, which results in not having a higher average energy as they strike the anode or the cathode resulting in increased spattering yields.

Studying the energies of electrons entering the negative glow region in a hollow cathode glow discharge without the presence of these different populations,<sup>7,8,10</sup> as opposed to the planar cathode glow discharge, where most authors refer only to the fast and slow electrons. In the hollow cathode glow discharge, the very fast beam electrons enter the negative glow after having been accelerated across the entire cathode drop without having undergone any (or many) multiple reflections. Therefore, they have energies comparable to the full cathode fall potential ( $> 150 \text{ eV}$ ). They are responsible for the secondary processes in the negative glow. The fast or secondary electrons arrive in the negative glow with much less energy than the beam electrons. This population of electrons derives from ionization processes at the beginning of the negative glow and has a range of energies from 0-15 eV. Finally, there are the plasma electrons. These are the electrons which have become thermalized to the temperature of the plasma through multiple surface collisions. These electrons are the most abundant group of electrons in the negative glow and are responsible for much of the cathode

The geometry of the cathode has no effect on the behavior of the electrons. It has been found that the mean free path of the electrons in a hollow cathode glow discharge is on the order of the diameter of the cathode cavity.<sup>10,11</sup> Because of this, many of the high energy beam electrons cross the negative glow cathode face and enter the cathode shield on the opposite side of the hollow cathode. Once inside the cathode shield, these electrons reverse direction and are re-injected into the negative glow resulting in multiple passes through the region. It has been shown that the beam electrons oscillate between the walls of the cathode, undergoing repeated cycles of emission while confined in the cavity. After a time, they decelerate and eventually diffuse to the walls.<sup>11</sup>

The geometry of the hollow cathode also affects the species reaching the cathode surface. In planar glow discharges, one of the processes by which an electron is emitted from the cathode surface is photoemission. Photons emitted from the glowing regions of the discharge are not affected by electric fields and therefore have a small chance probability of reaching the cathode surface depending on the area of the planar cathode. With the hollow cathode configuration, there is only a small chance that a photon will travel anywhere but to the cathode surface. With a hollow cathode glow discharge, the negative glow clearly has more contact time with the surface of the cathode. Also, the hollow cathode discharge is much brighter than the planar glow discharge, consequently, more photons are produced. It has been shown that photoemission can be a major

coincidence in secondary-electron spectra from the cathode,<sup>123</sup> the likelihood of a plasma striking the surface of the cathode increases from 0.3 in a planar cathode glow discharge to 0.8 in a hollow cathode glow discharge.<sup>12</sup> Not only are photons more likely to strike the surface of the cathode but back diffusion of analytic particles emitted in the cathode dark space is also greatly enhanced using the hollow cathode configuration. This is due mainly to the increase in electron impact collisions and is tightly dependent upon gas pressure. The cathode geometry traps all the species present in the cathode dark and negative glow regions within the hollow - electrons, ions, atoms, molecules, photons<sup>124</sup> - increasing the residence time in the analytical zone. The escape rate for rare gas and analytic species is less than 20% that of a planar cathode glow discharge system.<sup>12</sup> Furthermore in the planar cathode glow discharge, the negative glow region of the hollow cathode glow discharge is governed by unipolar diffusion. The difference is that the ions which diffuse radially in the planar cathode glow discharge are lost to analysis on the walls of the chamber, whereas the ions which diffuse radially in the hollow cathode glow discharge diffuse to the cathode dark and are subsequently accelerated to the cathode walls by the strong electric field, making them available for ionization.<sup>12</sup>

The current density within the hollow cathode glow discharge has been shown to be non-uniform and concentrated toward the bottom of the hollow.<sup>125</sup> Such a current density profile increases the sputtering rate.<sup>126</sup>

Overall, it has been found that the increase in the emission signal using the bipolar cathode configuration can be attributed to an increase in ionization in the negative glow, an increase in photoionization of secondary electrons from the cathode surface, an increase in random times of analytic species, and an increase in sputtering rates and analyte vapor concentrations.

### **Microcavity Hollow Cathode**

In Chapter 1, section 1.3, an overview of sputtered enhancement techniques for the hollow cathode glow discharge was presented. One of the most promising techniques mentioned was the use of a microcavity hollow cathode. This technique was used to offer a few orders of magnitude improvement in detection limits over conventional hollow cathode glow discharges. The work presented in this subsection makes use of the microcavity hollow cathode. With some understanding of hollow cathode glow discharges, it now seems appropriate to examine the microcavity hollow cathode in more detail.

Clearly, the same basic properties and characteristics of the hollow cathode glow discharge apply to the microcavity hollow cathode glow discharge. Several have shown that with the reduced diameter, the effects are even more pronounced.<sup>17-19</sup> First of all, the smaller cavity increases the analyte concentration in the negative glow region. There is also an increase in pressure within the hollow. It has been shown that the product of the pressure,  $p$ , and the diameter of the cavity,  $d_c$ , is a constant,<sup>1-19</sup> so that as the diameter decreases, the pressure

increases. The smaller cavity size means that there will be a thicker cathode sheath, resulting in a greater effect of the electric field on the cathode sheath space. From this, increased sputtering rates can be expected along with a more concentrated sputtered material.

All of these observations are valid but do not account for the dramatic increase in emission intensity when the diameter of the cathode is reduced, for example, from 3 mm to 2 mm. The same dramatic increase in emission intensity is not observed when the diameter of the hollow is reduced from 3 mm to 1 mm or from 4 mm to 3 mm. The "microcavity effect" is only observed in hollows less than 2 mm in diameter with a length-to-diameter ratio of at least 3:1. Unfortunately, there has been no theoretical treatment of the microcavity effect in the literature and, as, the phenomena remains unexplained.

#### Excitation and Ionization Processes in the Hollow Cathode Glow Discharge

The negative glow region of the hollow cathode glow discharge is the most important region for spectral analysis. Ground state atomic ions sputtered from the surface of the cathode are available for excitation or ionization by a number of different processes.

The principal mechanism responsible for excitation occurs by way of electron impact processes with efficiencies of low to moderate energy.<sup>11</sup> The mechanisms which result in ionization are more complicated. In some parts of the discharge, electron impact by high energy electrons creates ionization. In other

parts, reionization can be due to charge transfer reactions or to Penning ionization by metastable rare gas atoms<sup>10,11</sup>. Table 3-V<sup>1</sup> summarizes some of the important excitation and ionization processes that occur in the negative glow region.

Table 3-2. Glow Discharge Excitation and Ionization Mechanisms

EXCITATION	
Electron Impact	$A \text{ (or } X) + e \rightarrow A^+ \text{ (or } X^+) + e$ $A^+ \text{ (or } X^+) + e \rightarrow A^{++} \text{ (or } X^{++}) + e$
Photionization	$A \text{ (or } X) + h\nu \rightarrow A^+ \text{ (or } X^+)$
IONIZATION	
Penning	$X^+ + A \rightarrow X^+ + 2e$ $X^+ + A^+ \rightarrow X + A^+ + e$ $X^+ + A \rightarrow X + A^{++} + e$ $X^+ + A^+ \rightarrow X^+ + A^+ + e$
Charge Transfer	$X^+ + A \rightarrow X + A^+$

$X^-$  = rare gas atom

$X^0$  = rare gas metastable atom

$X^+$  = rare gas ion

$X^0$  = excited rare gas atom

$A^-$  = analyte atom

$A^0$  = analyte atom

$A^+$  = excited analyte atom

$A^{++}$  = excited analyte ion

## CHAPTER 3 DESIGN AND PARAMETRIC EVALUATION OF A MICROCAVITY HOLLOW CATHODE GLOW DISCHARGE EMISSION SYSTEM

### Chamber and Cathode Design

In approaching the task of designing a glow discharge chamber incorporating a microcavity hollow cathode, the goals of the design strategy had to be developed and evaluated in light of previous and current research in the field. The first goal was to reduce the physical size of the chamber itself. Previous work performed in our laboratory<sup>12</sup> using a 6 way stainless steel vacuum valve (100 mm<sup>2</sup> aperture) in the glow discharge chamber concluded that the large chamber volume contributed greatly to analyte vapor dilution. It was observed that, upon ignition of the discharge, the ions closest unambiguously diffused away from the plasma cathode to the walls of the chamber, decreasing the concentration of the analyte species in the plume volume of the glow discharge laser excited ionizer fluorescence system. Danco<sup>13</sup> recommended construction of a new glow discharge chamber to increase the concentration of the analyte vapor close and to reduce diffusion of the analyte away from the cathode. Although this recommendation was applied to a plasma cathode/glow discharge-in-seeded approach to investigating a reduced chamber size for the proposed microcavity hollow cathode

glow discharge plasma emission system. The smaller chamber size it was theorized, might favorably alter the different dynamics both internally and externally for the microtron hollow cathode glow discharge. It was decided that the new chamber would be approximately one third the volume of the chamber used in Beams's work. Since Beams made some comparison measurements using a hollow cathode as well as some dissociation measurements using a plasma entirely with the large chamber, a direct comparison could be made to determine if the reduced size of the chamber influenced the analytical figures of merit.

The second goal of the chamber design plan was to build an inexpensive, simple to operate, emission source, so that modifications, should they become necessary, could be made easily and inexpensively. It was determined that the chamber and cathodes could be made by modifying 1922 and 1938 pyrex tapered joints. The outer joint could be flattened into the chamber and the inner joint could be made into a cathode. These tapered joints fit snugly together, allowing the vacuum sealants to be used.

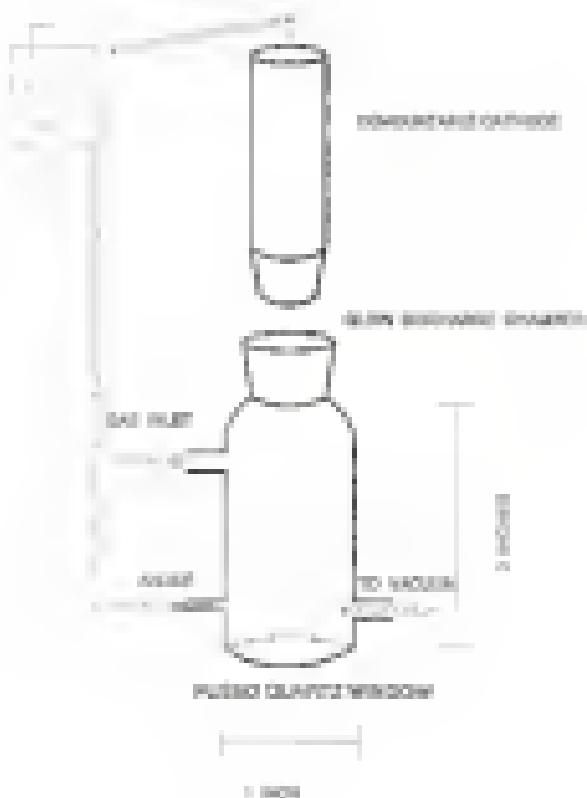
The next thing to consider was the placement of the gas inlet, the emission outlet and the anode. The vacuum outlet was placed at the end of the chamber next to the viewing port. Since this would increase the gas flow close to the window, it was hoped that this arrangement would help to prevent or reduce sample deposition on the viewing window. The anode was placed opposite the viewing port and was positioned to avoid physically obscuring the emission signal.

The placement of the gas inlet took a little more thought. Traditionally, the gas inlet has been placed transverse and parallel with the viewing window. This allowed the stream of carrier gas to flow across the window surface in an effort to prevent or reduce sample deposition on the viewing window. Many chambers incorporate this design (Bartovitch, 1970). However, Cough<sup>12</sup> developed a gas assisted glow discharge in which he changed the position of the gas inlet. His glow discharge chamber design positioned the gas inlet very close to and parallel with the surface of a plasma cathode in prevent sputtering from depositing on the cathode surface. Since that time, the gas assisted glow discharge has been utilized by a few investigators with good success.<sup>13-15</sup> They found that this configuration increased sputtering rate and transport of sputtered species away from the cathode. They also found that back sputtering onto the cathode surface was reduced. It was decided to incorporate this design feature in the new microcavity glow discharge emission system. Since the sample sizes which were to be analyzed would be less than 200 µg, for the largest of the samples, it was predicted that sample deposition on the chamber viewing window would only be a minor problem. It was felt that it was more important to make every effort to maximize sputtering rates so that the sample would be completely removed in as short a period of time as possible.

#### Figure 3.1 is an illustration of the new chamber design.

The last goal of the new design involved the microcavity hollow cathode. The cathode had to be easily removable and interchangeable to replace the

*Figure 3-1. Schematic diagram of glow discharge chamber*

**POWER SUPPLY**

sample analysis procedure. Figure 3-2 illustrates the design of the cathode that was finally selected upon. Each metal microtomy hollow cathode would first be machined to specifications ( $0.5 \times 10$  mm dia.  $\times 6$  mm deep). The metal microtomy cathode would be spinned onto a ceramic sleeve fabricated from machinable alumina. The ceramic sleeve would electrically isolate the metal cathode and confine the discharge within the cavity. The ceramic-sheathed metal cathode would then be spinned onto a TiWM pyrex glass tapered joint and would be fitted with an appropriate electrical connection to the negative pole of the high voltage power supply. It was felt that these cathodes would prove to be easy to make and easy to ignite.

The performance of the first chamber and cathode design was very good, but there was a problem with overheating of the cathode. After just a few minutes of continuous use, the cathode would heat up too much, causing the ceramic to expand and crack; the pyrex glass tapered joint. Eventually, the chamber cracked and broke as well. A new chamber was fabricated from a quartz (95%) glass tapered joint and new cathodes were built using quartz TiWM glass tapered joints. The basic design of the chamber and cathode remained the same.

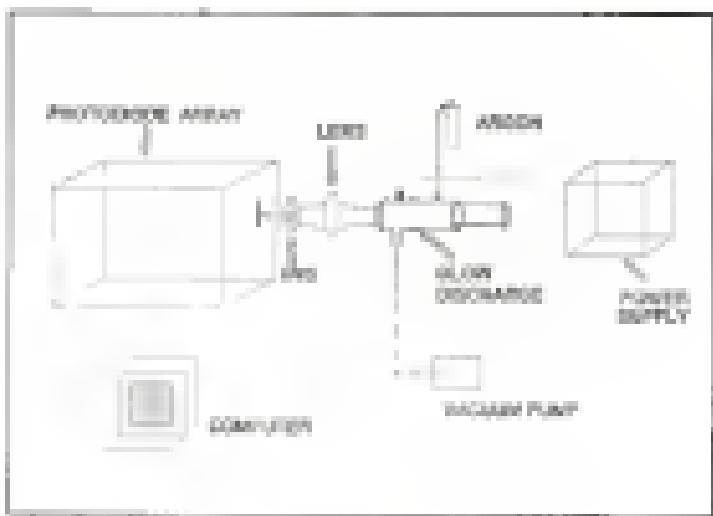
#### Experimental Setup

A schematic diagram of the experimental setup is presented in Figure 3-3. As can be seen from this diagram, the experimental setup is a simple one. The entire arrangement, in fact, fits on one  $4^{\prime} \times 6'$  optical bench.

Figure 3-2. Schematic diagram of the microscopy before collect



**Figure 3-5.** A schematic diagram of the experimental setup



The undistorted hollow cathode glow discharge source, which is the heart of the project, was mounted with a sturdy laboratory constructed fixture and holder in an x-p-e stage to simplify the alignment procedure. The cathode was connected to the negative terminal of a high voltage power supply (Hippocratecs, Inc., Model 600-210, Brewster, NY) which ranged in voltage up to 1000 V and current up to 400 mA. The anode, machined from stainless steel, was spotwelded into a 7/16 square copper tapered post bush into the glow discharge chamber and was electrically grounded. In order to limit the current going through the discharge and improve discharge stability, a 311B Hall current sensor was connected in series with the power supply. A laboratory constructed supply switch, which enabled remote operation of the glow discharge, was also connected to the power supply.

A dual stage rotary pump (Leybold Heraus Vacuum Products, Inc., Model Type A, Report, PA) was used to evacuate the glow discharge chamber. A capacitance manometer was used for monitoring the chamber pressure. Argon, the carrier gas used in these studies, was supplied to the glow discharge chamber via a gas inlet located near the cathode. The argon flow into the chamber was regulated at 2 mL/min with a precision needle valve. A pressure gauge was positioned between the needle valve and the argon tank so that the pressure in the needle valve could be controlled separately from the argon tank pressure.

To provide some external cooling to the cathode, a length of 1/8 inch x 1/16 inch Tygon tubing was connected to a flowing chilled water supply and wound around the outside of the chamber neck where the cathode is located.

Complicated optics were unnecessary to collect spectra. The emission output of the mercury glow discharge was focused onto the entrance slit of the spectrometer through a 3" focal length planoconvex lens. An aperture, reduced to the size of the focused beam, was placed directly in front of the spectrometer slit to prevent stray light from reaching the detector. Occasionally, neutral density filters were used, and when this was necessary, they were inserted in front of the aperture.

The wavelength dispersive system used in the project was a 1-meter spectrometer (Optis-Vac model HU1800, Princeton, NJ - 2400 gr/mm), having dispersion of 0.5 nm/mm. The detection system was an uncooled photodiode array (Princeton Instruments Inc., OEMA Model 184-1024, Princeton, NJ). Data acquisition and processing are controlled with the use of a personal computer and OEMA 8-128 software. With this instrument, the signal can either be integrated over a selected period of time or a selected number of scans can be accumulated. If desired, both integration and convolution can be performed on the same signal.

## Parametric Evaluation of a Microcavity Hollow Cathode Glow Discharge System

As with any new analytical system, the microcavity hollow cathode glow discharge emission system used in this work needed to be optimised. The various parameters essential for ensuring peak performance of the system were defined and a series of optimisation experiments were performed. The project proceeded for investigation of the microcavity hollow cathode glow discharge as a source for simultaneous multielement analysis of discrete solution samples of selected metals. There were to be two phases of the study. The first phase was designed to determine if the microcavity hollow cathode glow discharge was an effective source for ultratrace analysis. In this phase, the strongest emission lines from two elements, Pb and Cu, were to be investigated separately using cathodes of different form and materials. In the second phase, the microcavity hollow cathode glow discharge was to be investigated as a multielement source and simultaneous determination of Pb, V and Cr was to be attempted. Chapter 5 will present the optimisation procedure and results for the multielement studies. The optimisation studies for the single element phase of the project will be presented below. Where necessary, a simpler optimisation procedure has followed.

### Pressure, Voltage and Current

In a glow discharge operating at the observed regime, there is an interdependence of pressure, voltage and current. Only two of these parameters

may be varied at the same time. Because the high voltage power supply used in these experiments is a voltage-controlled power supply, the measurements of this study were made by either holding the pressure constant and varying the voltage or by holding the voltage constant and varying the pressure. Since the current could not be controlled, it was always one of the variables.

It was important to approach the optimization of the pressure, voltage and current systematically. The physical processes within the glow discharge are so complex that every change of the cathode and chamber has an effect on the stability of the discharge and the intensity of the emission signal. The optimum pressure and voltage for one particular measurement could well be different for another one. Therefore, separate optimization studies were performed for different analyses, different cathode materials and different cathode geometries.

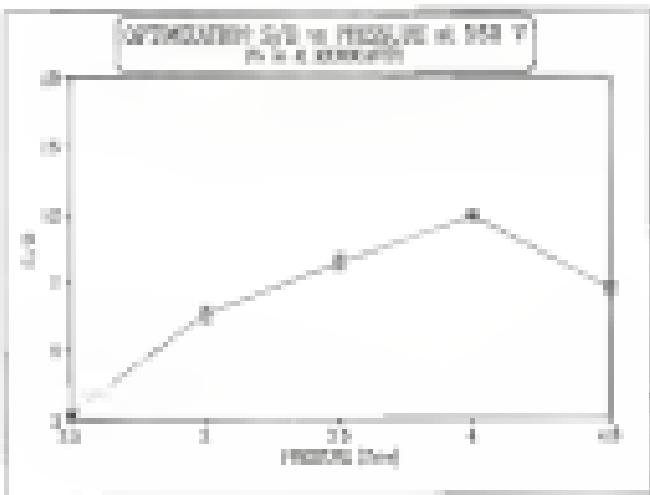
Four different cathode materials were evaluated: W, Ti, Al and Cu. Since tungsten is a hard metal and has a high melting point, it was hoped that it would prevent sputtering of the analysis residue off the cathode surface but not be powdered itself. If this were to happen, the emission spectrum would be free of cathode material signature lines, which could often cause severe spectral interferences. Unfortunately, tungsten proved to be an inappropriate cathode material for the project. Although a very stable, brilliant discharge was able to be initiated at 800 V and 2.5 Torr, the cathode overvoltaged almost immediately. In addition, rotation from the blank photocathode showed a sizable Cu signal due to

contamination in the aerosol. It also proved to be a poor cathode material for Pt analysis. After many attempts and many adjustments, only an insignificant signal was detected, and that was for a 2  $\mu\text{g}$  sample. The tungsten cathode was abandoned. Initial studies of the other three cathode materials looked promising, so pressure, voltage and current optimization of Ti, Al and Cu microscopy hollow cathodes presented.

The first set of optimization experiments were performed with Pt as the analyte. Figures 3-4 through 3-9 show plots of the signal-to-background ratio ( $S/B$ ) vs. pressure at a series of constant voltages. In all cases, the sample size was 100  $\mu\text{g}$  of Pt on the Al microscopy hollow cathode. The range of voltage was dictated by plasma stability. The range of pressure was determined by sample optimization. Over the range of pressure was determined, replicate measurements (at least 10) were taken at 0.5 Torr intervals. The error bars in these plots, as well as all other plots, represent  $\pm 1\sigma$  standard deviation from the mean. The results from this study indicated that the optimum voltage and pressure for Pt at the Al microscopy were 430 V and 3 Torr, respectively, resulting in a current of 62 nA.

At this point, it is important to explain exactly what the signal-to-background ratio represents in these plots. The lead emission line that was used was 400.76 nm. The Pt emission signal at this wavelength is defined by the photodiode array over a range of several debye, with a signal maximum at a

Figure 3.4 A plot of  $\Delta V$ -vs pressure at 500 V for 100 mg Pt in the Al matrix.



**Figure 3-5** A plot of %I vs pressure at 240 °C for 100 ng Pb on the Al substrate.

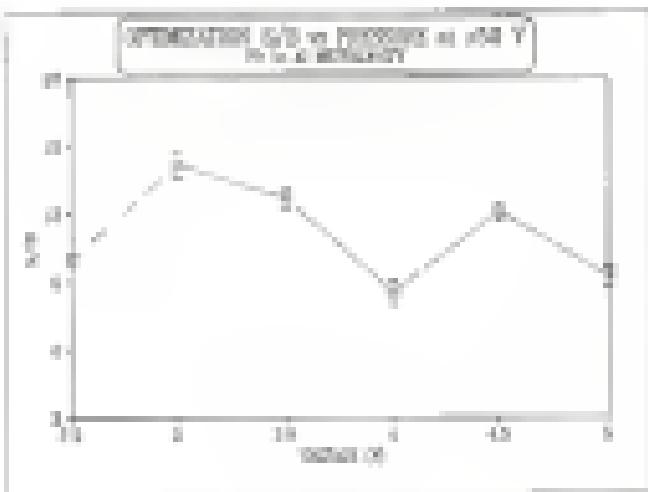
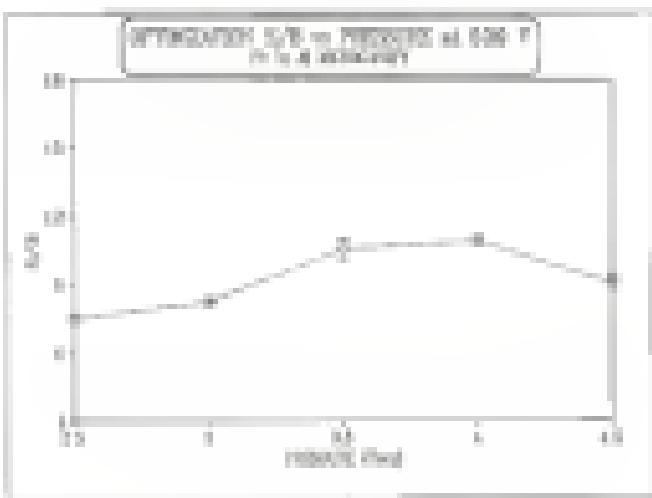
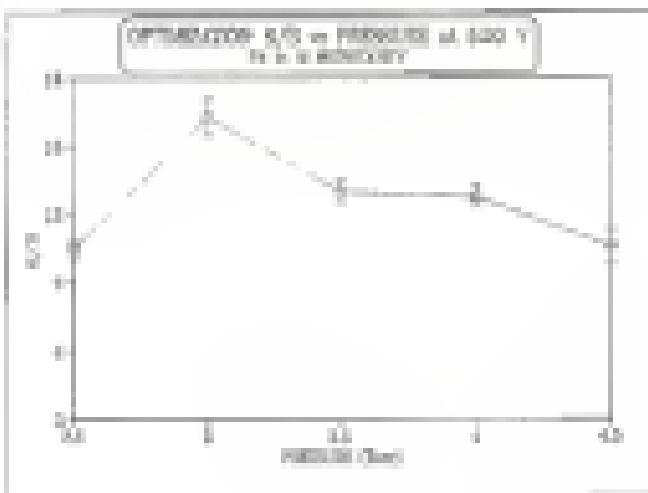


Figure 3-6 A plot of  $\Delta V$  vs pressure at 600 °C for 100 mg Pb on the Al monocrystal



**Figure 3.7** A plot of S/N vs. pressure at 600 V for 100 ng Pt in the Al microscopy

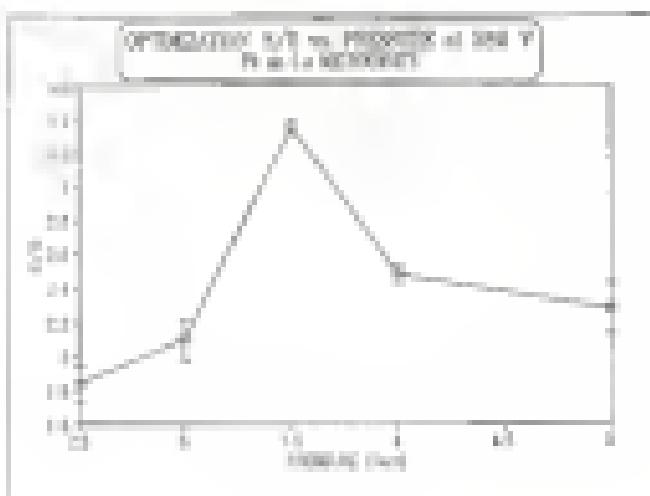


particular diode. As long as the wavelength setting on the spectrometer remains unchanged, the same diode will correspond to the 405.79 nm emission line each time a spectrum is taken. Once this diode had been determined, a series (usually 10) of blank measurements were taken. Each blank consisted of a volume of distilled water equal to the volume of Pt solution to be analyzed. The blank analysis was conducted under the same discharge conditions as the analyte. The signal for each blank at the lead diode was recorded. The average signal at the Pt diode for the 10 blank measurements was calculated. This was the signal due to the blank. Then, replicate measurements (at least 3) of Pt solution unknowns were taken and the average of these signals was calculated. The signal represented in the signal-to-background ratio was the net signal, the average analytical signal minus the average blank signal. The background measurement was taken as the average signal of 10 diodes to either side of the Pt emission line profile. Although not shown in the spectrum plots presented in this chapter, the signal-to-noise ratio followed the same pattern as the signal-to-background.

The pressure and voltage were also optimized for Pt in the Cu microtorrey hollow cathode for 0.7- $\mu$ g samples. Figures 3-8 through 3-11 show the plots of S/N vs. pressure indicating the optimum voltage and pressure of Pt in the Cu microtorrey to be 440 V at 3.5 Torr giving a current of 52 mA.

Next, a set of optimization experiments were performed for 0.6- $\mu$ g samples of Pt in a standard size Al hollow cathode (2 mm dia x 5 cm long). Figures 3-12,

Figure 3-8 A plot of the SR vs pressure at 580 V for 0.7 mg Pb in the Cu anode cavity



**Figure 3-6:** A plot of the S/N vs pressure at 600 V for 0.7 ng Pb  
at the Cu anode area

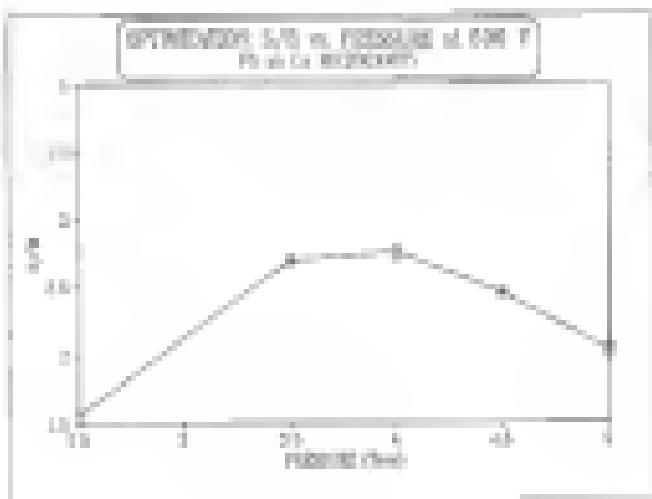


Figure 3 (B). A plot of the DB vs pressure at 400 V for 0.5 mol %  
in the Cu anode.

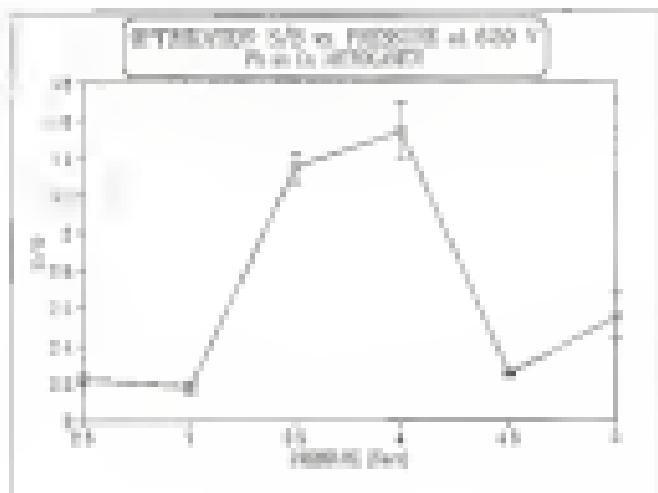
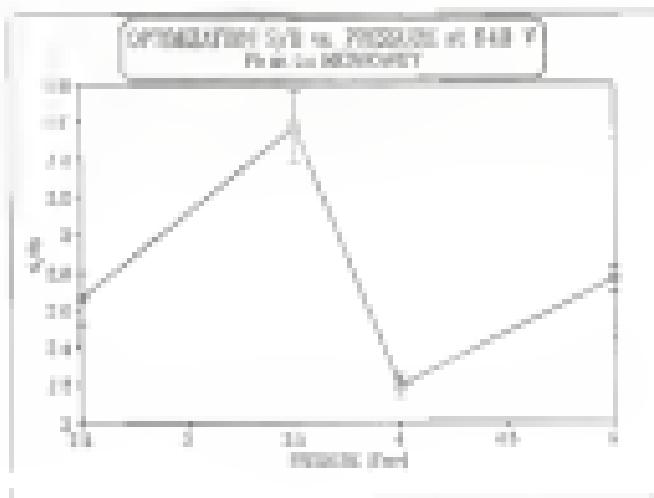


Figure 3.11 A plot of the OER vs pressure in kJ/mol for 0.7 mg Pb in the Cu anode cavity



through 3-14 show the results of this study where the optimum voltage and pressure turned out to be 600 V at 3 Torr with a resulting current of 46 mA.

Titanium was eliminated as a cathode material for Pt because it contained Pt oxidation.

The two cathode materials appropriate for the analysis of Cd were Al and Ti. The results of the experiments to optimize the pressure, voltage and current of 100- $\mu$ g samples of Cd in the Al microcavity are shown as plots (Figures 3-15 through 3-17) of %R vs. voltage at several pressures. These plots indicate that the optimum voltage and pressure for Cd in the Al microcavity are 600 V at 3 Torr. The current was 42 mA.

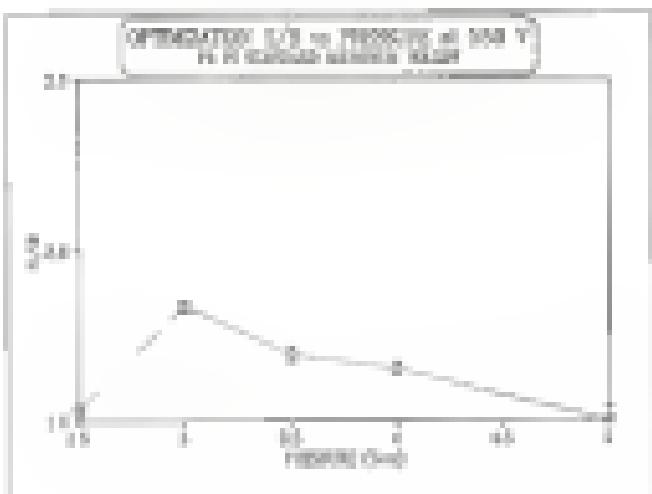
The same study was done for 100- $\mu$ g samples of Cd in the Ti microcavity hollow cathode and resulted in the best %R being obtained at a voltage of 600 V and a pressure of 3.5 Torr with a current of 33 mA. Figures 3-18 through 3-20 show the plots of %R vs. voltage at several pressures.

As can be seen from all these optimization experiments, it would not be difficult to determine optimum conditions universally applicable for the determination of all elements, perhaps 600V and 3 Torr.

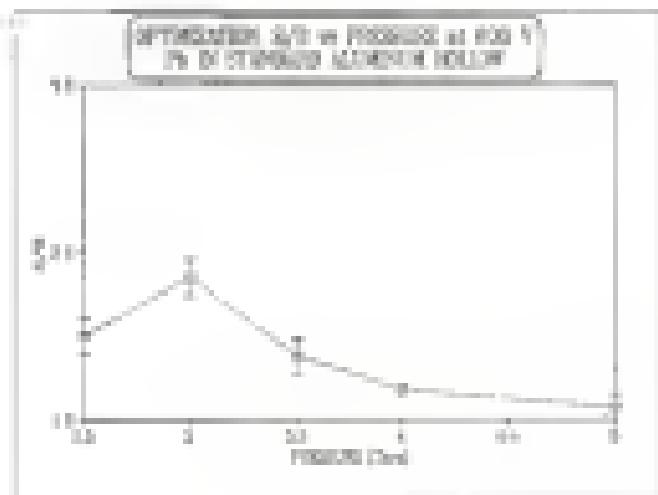
#### Chamber Pumping and Purging

Contaminants from condensates in the glow discharge chamber have been shown to have a significant impact on the fluorescence signal in a planar cathode glow discharge. For example, molecular bands from species such as OH, N<sub>2</sub>, CO

Figure 4-12. A plot of the ZAF vs position at 280 V for 0.1 mg Pb  
in standard. All hollow cathode.



**Figure 3-13:** A plot of the GSR as pressure is varied for O<sub>2</sub>/ng TiO<sub>2</sub> as standard. All hollow circles.



**Figure 3-14.** A plot of the drift vs pressure at 600 K for 0.1 mg Pb on standard Al foil vs volume.

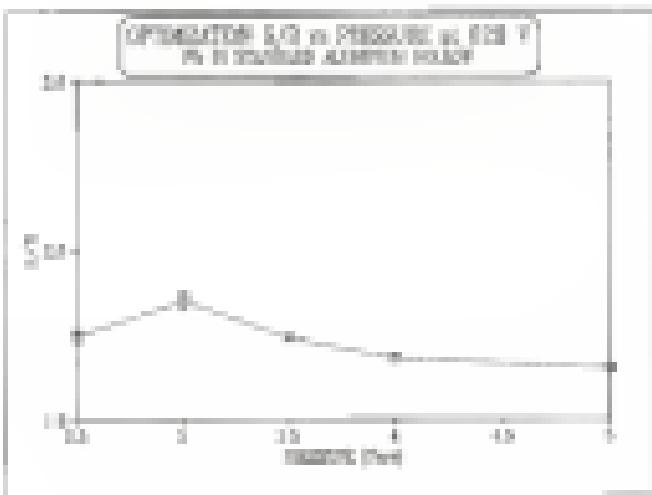


Figure 2-10 A plot of the S/N vs. voltage at 1 Torr for 200 mg Cu on Al substrate

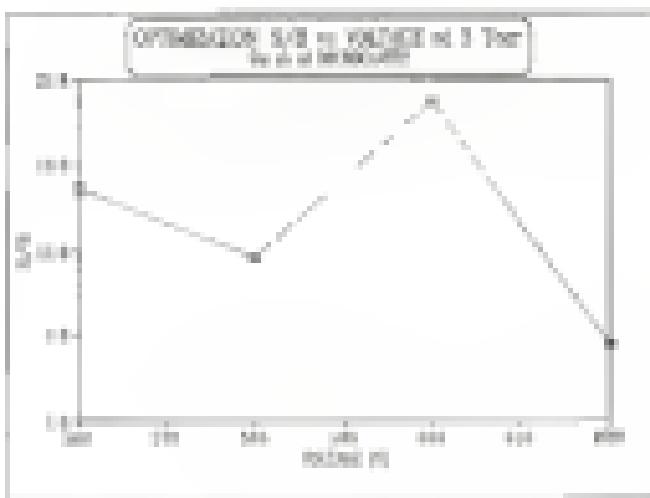


Figure 3-16. A plot of the NMR voltage at 2.9 Telsa for 200 mg Cu in oil microcores

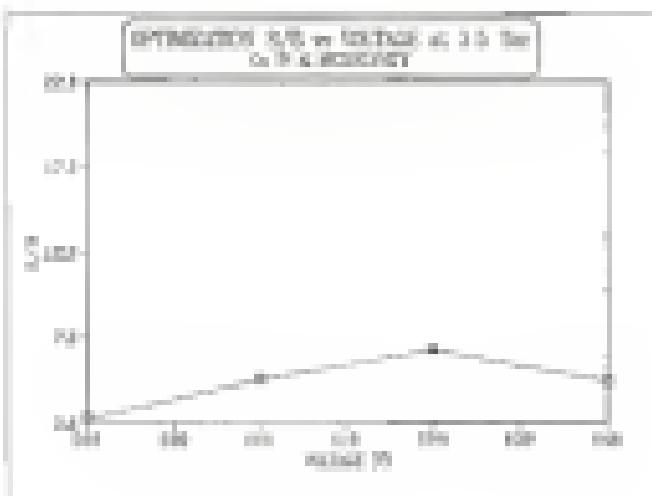


Figure 1.17 A plot of the S/I vs voltage at 4 Torr for 200 mg Cu in Al microscopy

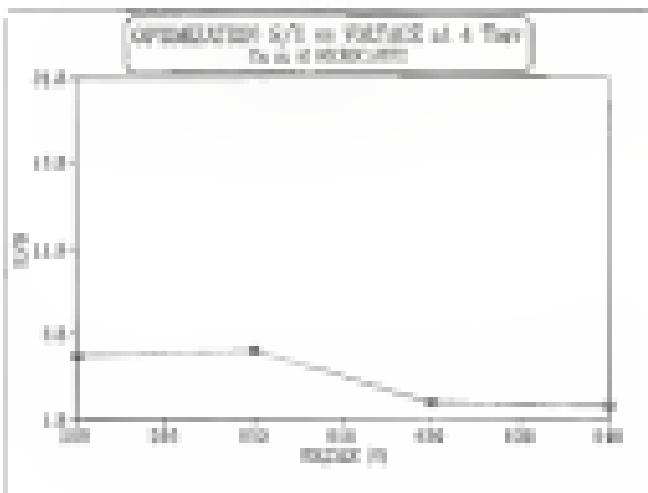


Figure 2.16 A plot of the DSC voltage at 2 °C/s for 100 mg Cu on Ti<sub>6</sub>Al<sub>7</sub>N<sub>2</sub>.

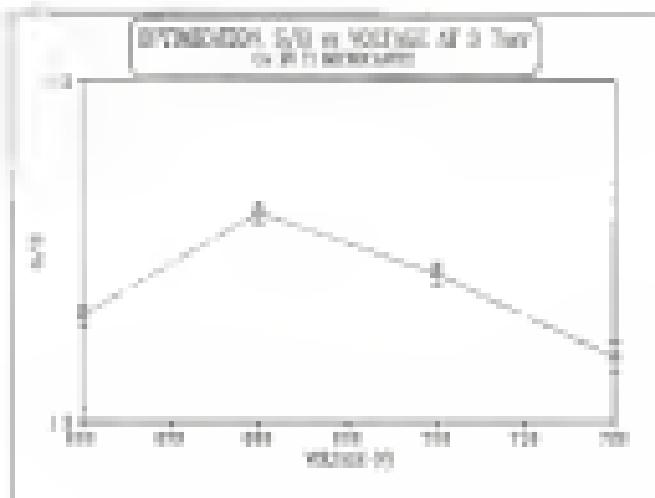


Figure 3-13 A plot of the S/B vs voltage at 2.2 Tm for 150 mg Cu on Ti respectively

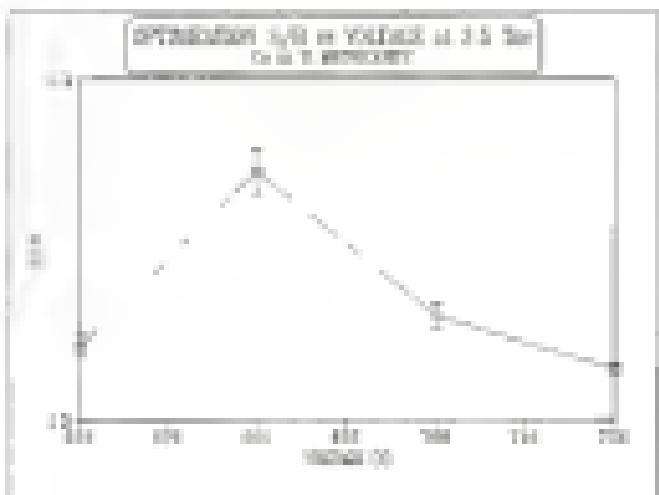
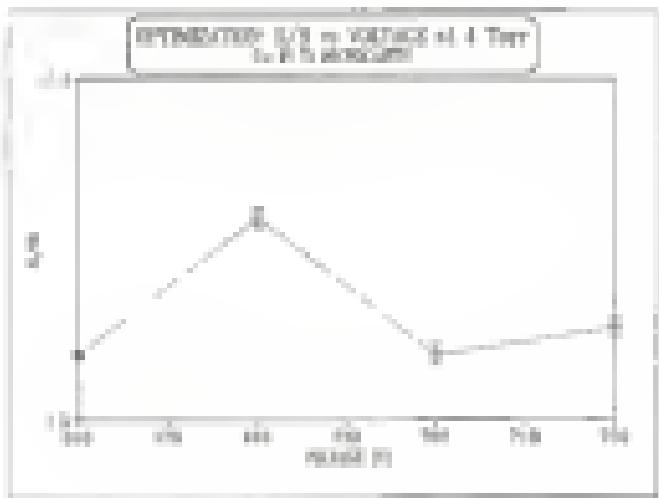


Figure 3-10 A plot of the S/B vs voltage at 4 Torr for 150 mg Cu  
at Ti wavemeter



and  $\text{CO}_2$  can degrade the analyzed spectrum dramatically. Another problem that occurs with atmospheric contamination is a low plasma discharge or sputter formation, which reduces the atom number density and causes a matrix.

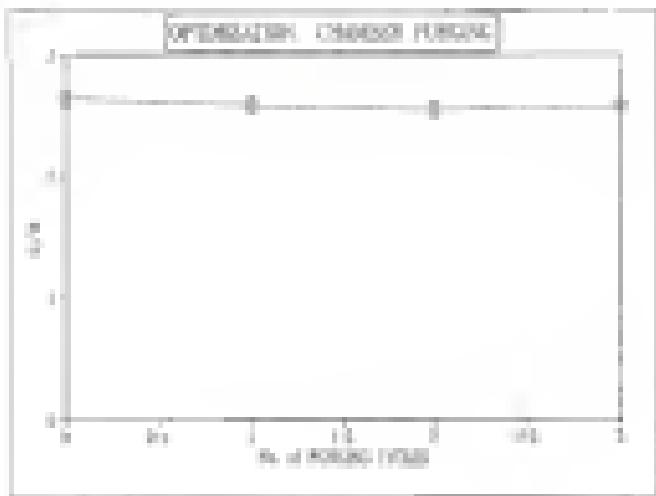
One method that has been suggested to reduce or eliminate atmospheric contamination is pumping and purging the glow discharge chamber. A study conducted previously in the laboratory indicated that the best fluorescence signal-to-noise ratio was obtained by twice evacuated the chamber to a mbar and introducing enough argon to bring the chamber to atmospheric pressure after each evacuation. The final pressure could then be set.

In order to determine if this procedure was necessary with the microstrip hollow cathode glow discharge emission system, a study was performed which measured the relationship between the signal-to-background ratio and the number of times the chamber was pumped down. The study was done for 10- $\mu\text{g}$  samples of Pb in the Al matrix. As can be seen in Figure 3.21, there was no significant difference in S/B indicating that atmospheric contamination was not a problem in glow discharge emission.

#### Sample Drying Time

Another parameter to be evaluated was the sample drying time. Almost every study involving the analysis of solutes matrices in a hollow cathode glow discharge system rejects the oven drying procedure. In most previous studies, the

Figure 3-11. A plot of S/S vs page cycles for 10 ug Th in *All microcentrifuge*



sample is dried near the cathode by placing the hollow cathode containing the solution under an infrared lamp until it is dry, anywhere from 3 to 10 minutes, depending on the size of the cavity and the size of the sample. Previous reports indicate that the sample should be completely dried to avoid contamination from water.

Initially, the procedure was followed. However, because the sample size at that time was 2  $\mu$ l., the sample was then half-filled the very small microanalytic hollow. It required 10 minutes under the infrared lamp to dry. Problems arose when the pyrex cathode would heat up excessively and either warp or crack, rendering them unusable. It was then decided to let the cathodes just air dry. This also presented problems. It took over 30 minutes for the sample to dry, which allowed time for an oxide layer to form on the walls of the cavity. When this happened, it was very difficult to remove the discharge. It was finally decided to dry the cathodes under a gentle stream of dry nitrogen for 10 minutes. This drying procedure worked well. The cathodes dried near the cathode and the discharge was easy to light and maintain.

As often happens in research, the importance of drying time was happened upon quite by accident. One day, in making a "quick-and-dirty" measurement on a sample that had only been drying for 1-2 minutes, the signal was, unexpectedly, a good three times that of any previous measurement of comparable mass. It was clear that phenomena had to be investigated. A study of the effect of sample

drying time on SSI was conducted performed. The results are shown in Figure 3-22, which plots the SSI vs the sample drying time for 400 ng Pb in the Al microscopy. From this plot, it is clear that the best signal-to-background ratio is achieved with only a minimum of drying time. Perhaps, it is the case that sputters from no matter what drying method is good, and that a larger population of free atoms is attainable when surfaces are not thoroughly dried. A similar study was done when tungsten and tungsten boride to be used. This study indicated that the best signal-to-background ratio was achieved when the sample was not dried at all. (See, 2002)

A very simple optimisation study of the SSI vs the extraction slit width of the monochromator was carried out. (Figure 3-23 shows the plot of SSI vs slit width for 200 ng Pb in the Al microscopy). The results indicate that the optimum slit width is 11  $\mu\text{m}$ . This study was also done for 10 ng Cu in the Al microscopy with similar results.

#### Cathode Precoating

Several authors have studied the effects of precoatinging the hollow cathode to maximize the emission signal and improve precision.<sup>17-21,24</sup> Consider mounting of the hollow cathode inside a cylinder with a flat bottom. These studies have shown that the sputtering process reshapes the hollow cathode from the original flat bottom to a spherical cavity. The walls of the hollow cathode also undergo a change. While the bottom is becoming spherical, there is a portion

Figure 3-21 A plot of  $\delta T$  vs drying time

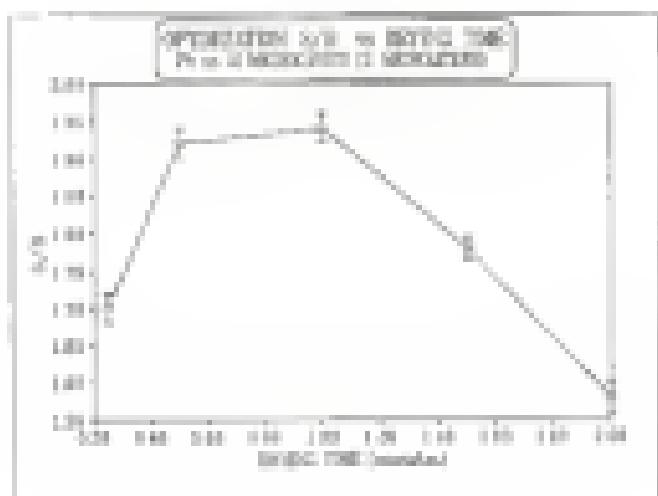
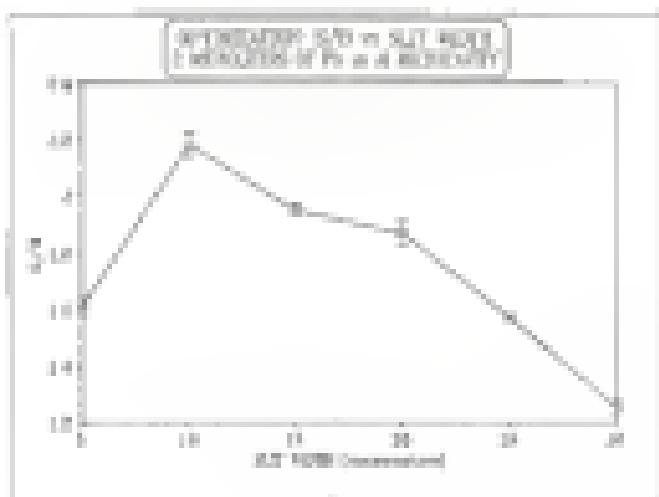


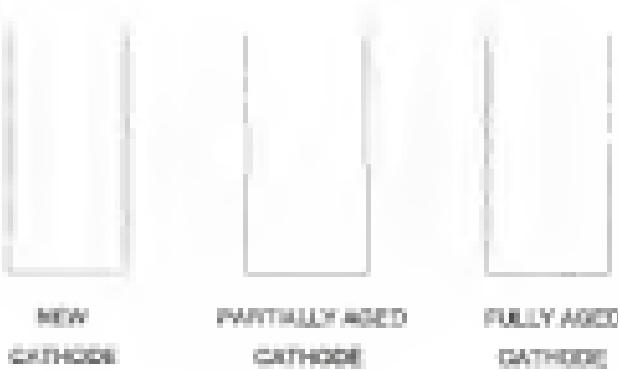
Figure 3.25 A plot of  $S/\theta$  vs. the width



along the wall which begins to contract. Figure 3-34 illustrates this process. It has been shown that the discharge is most stable when the cathode achieves this shape. In a recent study on cathode aging, Wilkins<sup>22</sup> claimed he achieved complete aging of a Cu macrocavity after 1000 1/2 s discharges.

This seemed a reasonable study to take note of, and it was decided that a similar aging procedure would be followed for the macrocavities in this project. To avoid overheating the cathodes, they were aged for 500 1/2 s discharges over a period of a few hours. Although this was presumed to be sufficient preconditioning, it was not. It was observed that after more than 1000 discharges beyond those required for aging, the Al macrocavity hollow cathode rapidly charged. The current to the discharge decreased by 50–70% for the same applied voltage and the same pressure. More importantly however, was the fact that the ionization increased dramatically. In reviewing Wilkins' study, it was clear that although a spherical bottom had been formed after 100 1/2 s discharges, the contraction at the wall had not formed. Pictures of his macrocavities show that even after 1500 1/2 s discharges the contraction was just beginning to be formed. What<sup>23</sup> has reported that optimum performance is reached when the ratio of the diameter of the specimen formed by the contraction to the diameter of the spherical bottom is 0.25. The abrupt change in the performance of the Al macrocavity hollow cathode may have come at the point where the particular hollow cathode achieved dimensional stability. For whatever reason, the best results (to be presented in Chapter 4) were obtained after the charge took place

*Figure 3.24* An illustration of coded aging



## CHAPTER 4

### SINGLE ELEMENT DETERMINATION OF COPPER AND LEAD BY HANDBAMPER SOLUTION RESIDUES BY MICROSCANNING HOLLOW CATHODE GLOW DISCHARGE

Evaluation of the microscanning hollow cathode glow discharge as a source for simultaneous multielement analysis of discrete particulate samples was carried out in two phases. Each phase was designed to answer a question. First of all, would the microscanning hollow cathode glow discharge prove to be a good source for simultaneous analysis of discrete particulate samples? Secondly, would the source be applicable to multielement determination? This chapter focuses on a series of experiments designed to answer the first question.

Two elements, Cu and Pb were chosen for these analyses. Each element was evaluated individually using its strongest emission line - 324.7 nm for Cu and 403.7 nm for Pb.

#### Experimental

The experimental setup used in the single-element residue experiments was described in Chapter 3. Calibrated coated density filters were used for all planned measurements. In addition, a 10 nm bandpass microscanning filter centered at 320 nm was used for the Cu determinations.

### Sample Preparation

The daily required sample preparation solutions of various concentrations of Cu and Pb were prepared by appropriate dilutions of 1000 ppm research grade standard solutions (Fisher Scientific) with deionized water. Volumetric flasks used in these preparations were thoroughly cleaned and rinsed in concentrated nitric acid.

Delivery of the sample solution onto the cathode was accomplished with the use of a micropipet. Initially, 2  $\mu$ L samples were used and were delivered with a calibrated 2  $\mu$ L disposable pipet that had an accuracy rating of 0.3% and a precision of 0.2%. Disposable pipet tips were used in all cases. Subsequently, smaller samples were delivered by a newly factory calibrated Keck micropipet, Model P-2 "Pipetman," using disposable metal-free pipet tips. This particular micropipet was calibrated to deliver volumes from 0  $\mu$ L to 1  $\mu$ L with precision ranging from 14.8 for volumes below 50  $\mu$ L to 0.3% for volumes above 500  $\mu$ L. The smallest volume used in this study was 50  $\mu$ L.

### Experimental Procedure

Over a period of several months and through much trial and error, an experimental procedure was developed which was consistent and effective. First, the spectrometer wavelength selector was set to the appropriate wavelength. Initial spectra were taken: 1) with the spectrometer slit closed; 2) with the spectrometer slit opened and the room lights off; and 3) with the slit open and the room

lights on. Analysis of these spectra gave an indication of the contribution of each set of cathodes to the spectral background. All cathodes were cleaned with 3% nitric acid prior to a day's work. The copper cathodes were cleaned for about 3 minutes while the Al and Ti cathodes needed to soak overnight. This removed a thin surface, which was verified by polishing the dry, clean cathode and analyzing the resulting spectrum. A series of blanks were run next. This consisted of one to fifteen individual spectra of fluorinated wear in whichever cathode was to be used for analytical determinations. A particular volume of fluorinated wear was deposited onto the cathode bottom and the cathode was inserted into the glow discharge chamber. The chamber was evacuated to about 1 mTorr and set to the appropriate pressure as measured by a capacitance manometer. The voltage was then set.

The data acquisition began prior to ignition of the discharge in order to record the baseline with the discharge off. The switch was then thrown and the discharge ignited. The 32' CRT monitor, which was used for data acquisition and processing, allowed great flexibility in setting the parameters of data acquisition. The signal could be integrated over a period of time or a number of scans with the same integration time could be averaged or a combination of the two could be selected. A previous study performed in our lab indicated that the spectrum signal-to-noise was achieved by integrating signals for longer periods of time rather than averaging spectra. The integration time for most of these experiments was set to

1 s, which represented integration over 30,000-s scans, and, subsequently, two spectra were averaged. The IST 120 software also enabled the behavior of the analytical signal to be observed over time. Either a single spectrum or a 3-D spectrum could be generated. Since this work was based on discrete sampling, the signal was transient and the 3-D plot was very useful in helping to determine if the entire sample had been sputtered off the cathode. Figure 4-1 shows an example of the temporal behavior of an analytical signal.

Once the data had been acquired, the discharge was usually switched off. Having acquired the data for the blank agents, the analytic samples were then determined in the same manner as the blank samples had been determined. The one difference was the necessity to perform cleaning etchbacks of the cathode to make sure any analyte that had redeposited on the cathode surface was sputtered off. In the case of Pb, this could take as long as three 30-second discharges. In all cases, care had to be taken as to not to overheat the cathode. The appropriate spectra were saved on floppy disk for further analysis.

#### Determination of Copper

Through a series of experiments, it was determined that Al and Ti cathodes should be used in the determination of Cu. The emission wavelength chosen for the analysis was 324.754 nm. The Al apparently proved to be the best cathode, providing a stable, reproducible discharge and a limit of detection superior to previous glow discharge emission work. Figure 4-2 shows the analytical

**Figure 4-1** An emission spectrum of Pb showing the temporal behavior of the signal

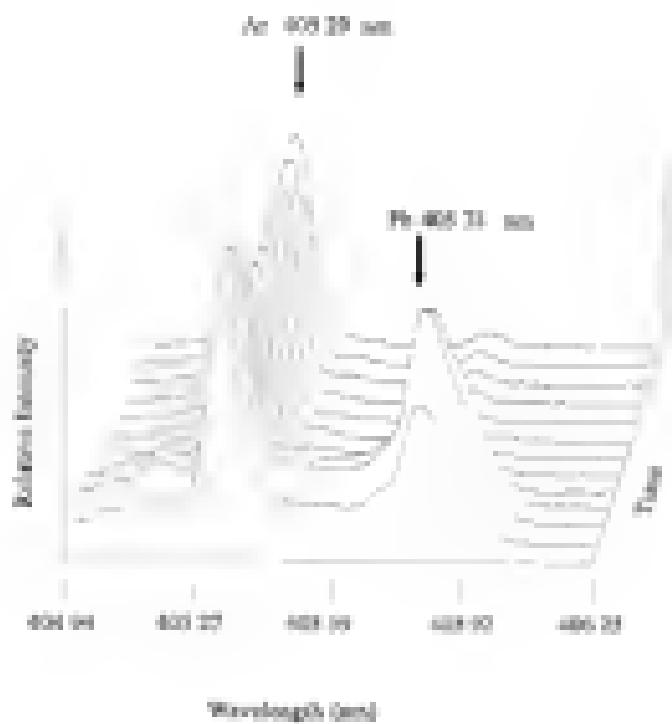
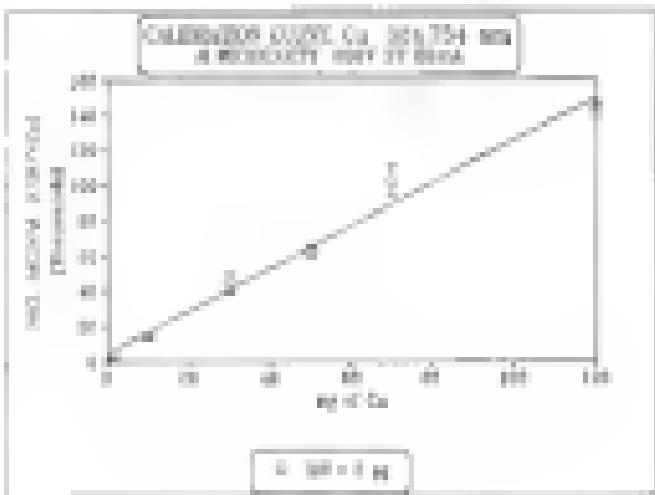


Figure 4.2: Calibration curve of Cu in the Al microarray at 104 T nm



calibration curve of Cu in the Al microcavity. The calibration curve, as well as all others presented in this chapter, was generated using peak heights. The net equivalent T ratio of the calibration curves represents the analytical signal less the signal due to the blank and less the baseline signal. The baseline signal was determined as the average intensity of 10 nodes on either side of the emission line away from the wings of the peak. The best fit line was generated by a linear least squares regression analysis.

The levels of detection in these analyses were determined using the  $3\sigma_{\text{blank}}$  method, with  $\sigma$  representing either the standard deviation of the blank signal or the standard deviation of the blank. The method most often reported in the glow discharge literature uses the  $3\sigma_{\text{blank}}$  method. For the analysis of Cu in the Al microcavity hollow cathode the limit of detection based on  $3\sigma_{\text{blank}}$  was calculated to be 2  $\mu\text{g}$ . The more conservative approach,  $3\sigma_{\text{blank}}$ , gave a limit of detection of 13  $\mu\text{g}$ . The correlation coefficient,  $r^2$ , was 0.992 and the log-log slope was 0.992. This was based on experiments in which increasing volumes of the same concentration of solution were determined. The same process was reported by sampling equal volumes of differing concentrations. There were no significant differences in the figures of merit for either method of sample delivery. The precision, based on at least 3 replicate measurements, of the Cu analysis ranged from 11% to 17% RSD and the calibration curve was linear over 3-3 orders of magnitude.

Cu was also determined using a Ti monocrystalline hollow cathode. These experiments were fraught with difficulties. The Ti cathode proved extremely temperamental. It was very difficult to attain a stable plasma. The cathode would also burn up very rapidly. In such a manner effort to obtain any reasonable analytical data. Figure 4-3 shows the calibration curve for Cu in the Ti monocrystalline. The limit of detection based on  $3\sigma_0$  was, however, a respectable 71 pp. The limit of detection based on  $3\sigma_0$  was 470 pp. The precision ranged from 2% to 16% RSD. The value of  $r^2$  was 0.976 and the log-log slope was -0.977.

In order to compare the results obtained using the monocrystal with those that would be obtained using a standard alumina hollow cathode, Cu was also determined using Al monocrystalline hollow cathode (Ceramco). The calibration curve is presented in Figure 4-4. The limit of detection for  $3\sigma_0$  was 1 pp and for  $3\sigma_0$  was 7 pp. In this case the  $r^2$  was 0.994 and the log-log slope was 1.021. The precision ranged from 5% to 13% RSD.

#### Determination of Lead

Through another series of experiments, it was determined that Cu and Al monocrystalline hollow cathodes could be used for the determination of Pb. The emission wavelength chosen for the analysis was 403.3 nm. Here, again, the Al monocrystalline hollow cathode proved to be the best cathode. A stable, reproducible discharge was easy to attain and to maintain. The cathode was not subject to

Figure 4.3 Coloration curve of Cr in the Ti environment at 124 °C

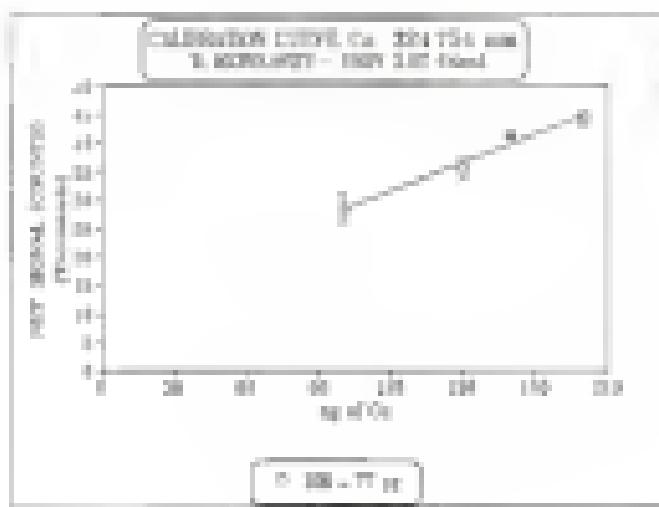
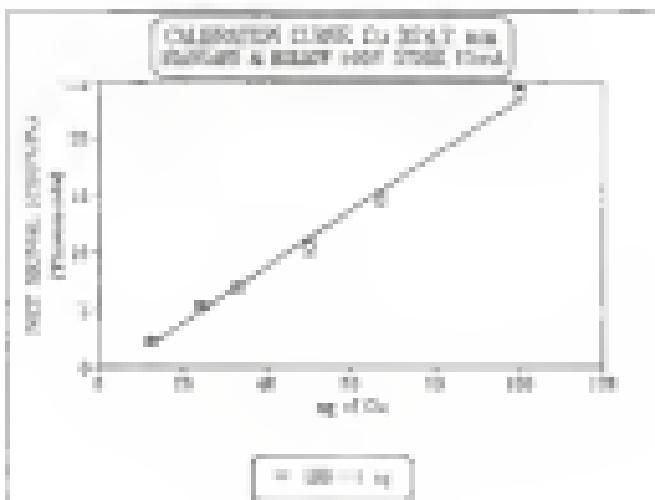


Figure 4-4 Calibration curve of  $C_V$  on the standard Al hollow at 104 T and



oxide heating problem. The limits of detection obtained for Pb using the Al macrocavity were far superior to previous glow discharge analysis work and, in fact, rivaled glow discharge fluorescence.

Figure 4-3 shows the analytical calibration curve for Pb in the Al macrocavity. As in the case of the copper analysis, comparable detection limits were obtained for sampling different volumes of the same concentration of solution and for sampling equal volumes of different concentrations. The calibration curve was reproducible from day to day and from one Al macrocavity to another of equal size. The detection limit for Pb in the Al macrocavity hollow cathode was 36 pg using the  $\text{Be}_6$  method and 146 pg using the  $\text{Be}_9$  method. The  $r^2$  value was 0.993 and the log-log slope was 1.112. The precision ranged from 7% to 23% RSD.

Pb was also determined in the Cu macrocavity hollow cathode. Figure 4-4 shows the analytical calibration curve for Pb in the Cu macrocavity. The  $\text{Be}_{10}$  limit of detection was calculated to be 1.8 pg and the  $\text{Be}_9$  limit of detection was 1.71 pg. Here, the  $r^2$  was 0.993 and the log-log slope was 1.142. The precision ranged from 7% to 15% RSD.

In order to show a comparison of the limits of detection of Pb in the Al macrocavity and the Al standard hollow cathode, Pb was determined in a standard (2 mm dia) Al hollow cathode. The calibration curve is presented in Figure 4-3. The limit of detection based on  $\text{Be}_{10}$  was 10 ng and the  $\text{Be}_9$  detection limit was 29 ng. The  $r^2$  value was 0.986 and the log-log slope was 1.306.

Figure 4-3 Calibration curve of Pb on the Al matrix at 495.75 nm

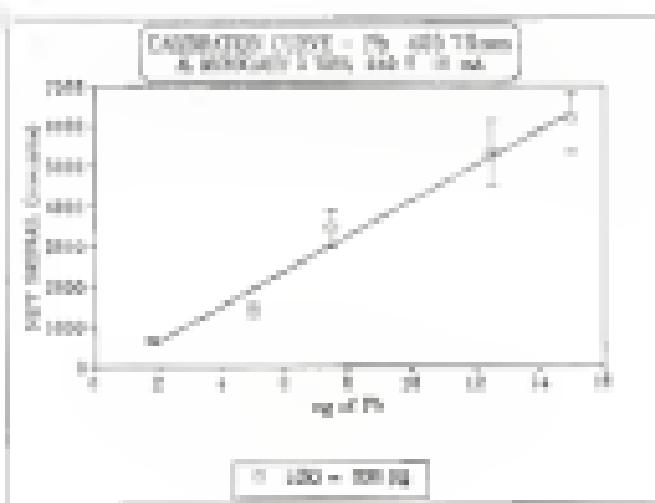


Figure 6.6 Calibration curve of Pt at the Cr wavelength of 481.11 nm

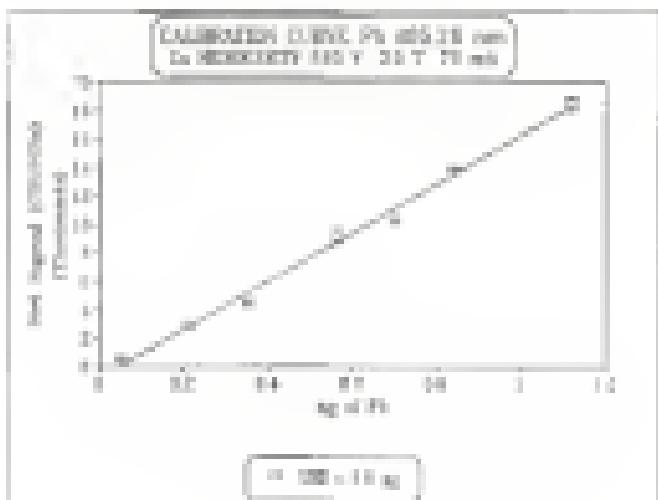
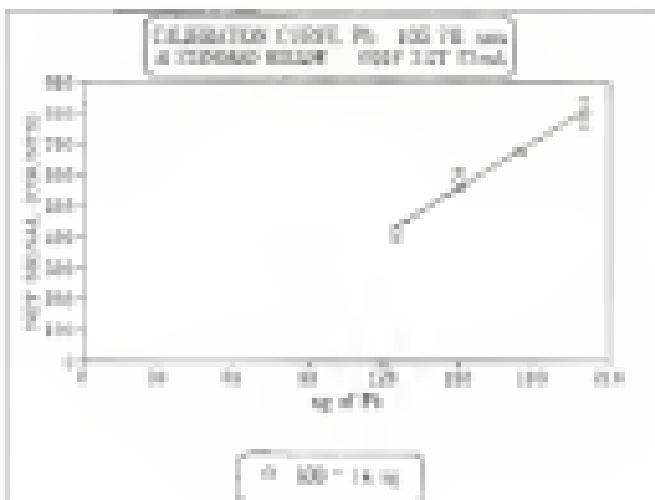


Figure 6.7 Calibration curve of Pt vs the standard Al hollow at 429 °C on



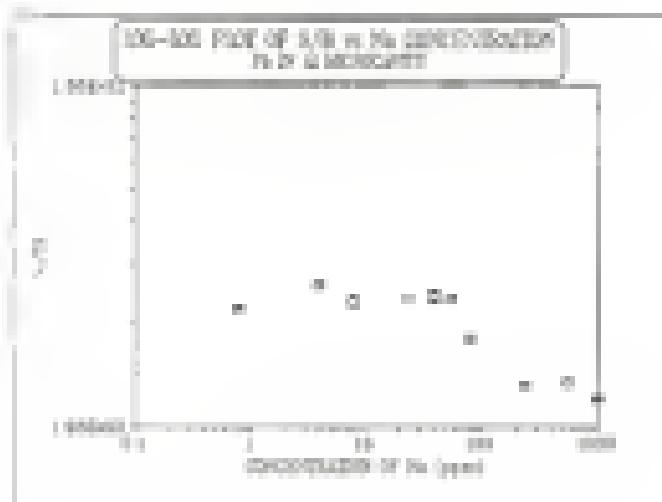
### *Effect of Na on the Analytical Signal*

In order to determine if there was any effect on the analytical signal from study secondary elements, a series of experiments were performed to ascertain what, if any, concentration of Na added to the analysis solution would suppress the analytical signal. Figure 4-8 shows a log-log plot of the S/N of Pb vs the concentration of added Na. As can be seen from this plot, there is no effect on the analytical signal. The suppression of the signal begins when the mass of Na is 100 times that of the analyte but is really pronounced when the mass of Na is greater than 300 times that of the analyte.

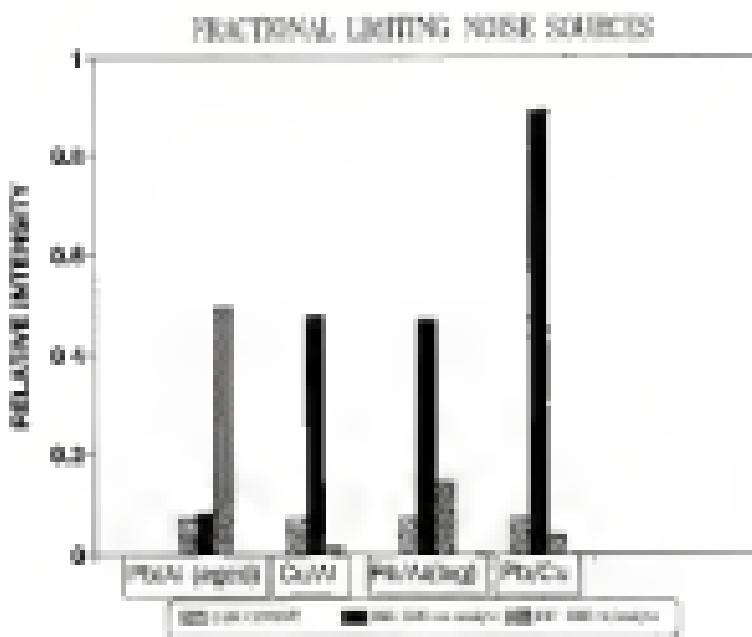
### *Limiting Errors*

No discussion of a new technique would be complete without a close look at the limiting errors of the system. Figure 4-9 is a graph which characterizes the different analytic voltage contributions based on the major sources-of-error. These errors can be categorized into three areas - dark current, background emission with a clean cathode and background emission when analyte is present. In most cases, the major contributor to the noise of the system is the background emission from the blank cathode with a small contribution from the background emission when analyte is present. However, in the case of Pb in the Al microcoating hollow cathode, there is a difference. Notice that the major contributor to noise is no longer background emission from the blank but is background emission from the analytical signal. This shift in the relative contribution of the errors may help

Figure 4-8 Log-log plot of ESR vs concentration of Na showing the effect of Na on the IPH analytical signal in the Al macrocycle at 400 GHz.



**Figure 4.9:** Graph showing the blanking ratios for each analyte-cathode combination. The signal intensities are normalized for the total noise in the worst case (Pt in the Cu measurement)



explain the extraordinary structuring a fully aged cathode. When<sup>12</sup> claimed that two dimensional stability was reached the dimension of the hollow porous structure and no aged driven lattice spreading and edgevation was reached. In such a stable configuration, the contribution of spreading of cathode material is decreased. The sample deposited on the cathode may be sputtered preferentially, thus explaining the increased contribution of the noise from sputter background emission. Even though the total noise in cases one and two (Pb on the aged Al microcavity and Cd on the newer Al microcavity) are comparable, the S/N is much greater in the case of the aged hollow. For a 15 pg sample of Pb on the aged Al microcavity and Cd on the newer Al microcavity, the S/N is comparable, the S/N is much greater in the case of the aged hollow. For a 15 pg sample of Pb on the aged Al microcavity, the S/N is 1040. For a 50 pg sample of Cd on a newer Al microcavity the S/N is 50. This represents a dramatic difference, however a better comparison would be to look at the S/N of Pb on a newer Al microcavity and on the fully aged Al microcavity. Experiments performed to analyze Pb on the Al microcavity hollow & had been completely aged resulted in a S/N, for a 15 pg sample, of 517. A better than twofold increase in signal-to-noise is achieved upon dimensional stability of the cavity.

#### Determination of Pb in Soil Samples

A complete evaluation of the microcavity hollow cathode as a source for trace and ultratrace analysis must include the evaluation of the accuracy of the method. The NIST standard reference material 1643b "Trace Elements in Water"

were chosen as the standard with which to perform this evaluation. The certified concentration of Pb in this standard is  $26.1 \pm 0.07$  ppb.

It was decided that the reference standard would be analyzed for Pb in both the Al and Cu microcoated hollow cathodes. The results were accurate within experimental error. Four replicate measurements of the checked reference material were taken and the Pb content in the Cu microcoated hollow cathode was analyzed. The results of these measurements determined the concentration of Pb to be  $25.3 \pm 3.4$  ppb. Three replicate measurements of the same standard reference material were taken using the Al microcoated hollow cathode. The concentration of Pb in the checked reference material with this cathode was  $26.1 \pm 3.8$  ppb.

#### Discussion

The results of these studies have been very promising. The microcoated hollow cathode glow discharge has been shown to be a good source for trace and ultratrace analysis for complex matrices samples. With a fully aged Al microcoated discharge the detection limits are achievable for Pb. Table 4-1 compares the results of these experiments with other glow discharge work. Also included in Table 4-1 are results of Pb and Cu analysis using other techniques.

Table 4-1 Absolute Detection Limits for Aspergers Cu and Pb Samples

	Cu (ppb)		Pb (ppb)	
	2 $\sigma_{\text{B}}/2$	3 $\sigma_{\text{B}}/3$	2 $\sigma_{\text{B}}/2$	3 $\sigma_{\text{B}}/3$
THIS WORK	2 $\sigma_{\text{B}}$	3 $\sigma_{\text{B}}$	2 $\sigma_{\text{B}}$	3 $\sigma_{\text{B}}$
Tl interassay	77	400		
Cu interassay			1.9	172
Al interassay	2	15	0.026	0.140
All standard hollow	1000	7800	14000	24000
OTHER GD WORK				
GD-Emission (quadrupole)	40 <sup>a</sup>		900 <sup>a</sup>	
GD-TSFS			3 <sup>a</sup>	
GD-AAS (pulsed)	3 <sup>a</sup>			
GD-Hyperion AAS	3 <sup>a</sup>		4000 <sup>a</sup>	
OTHER TECHNIQUES				
Cx Spark			5000 <sup>a</sup>	
dc AAS	3000 <sup>a</sup>		10000 <sup>a</sup>	
ETA-AAS	3 <sup>a</sup>		7.5x10 <sup>-4</sup> <sup>b</sup>	
ICP-AES (photoluminescence)	31 <sup>a</sup>		43 <sup>a</sup>	

In addition, experimental conditions can be set such that a stable discharge, easy to initiate and easy to maintain can naturally be achieved. Some other attributes of the microbattery bottom cathode include the lack of memory effects and long lifetimes. It was found in these experiments that the surface could be cleaned by repeated agitating until the baseline returned to its original value. It was also found that, if properly coated, the cathodes were very hardy and long-living. From this study, it is hard to predict the exact lifetime, but the oldest cathode has undergone over 1500 discharges and still gives good results.

## CHAPTER 5

### SIMULTANEOUS MULTIELEMENT DETERMINATION OF DISCRETE MICROSAMPLE ABSTRACTION RESIDUES BY MICROGAPITY HOLLOW CATHODE GLOW DISCHARGE EMISSION

This chapter will focus on experiments designed to determine if microcavity hollow cathode glow discharge emission is applicable to simultaneous multielement analysis.

Since the detection system used in these studies was a photodiode array with a 20 nm window, the process of finding a group of elements with emission lines sufficiently narrow, easily resolved from background emission lines and located within a 20 nm span was a tedious one. After many preliminary experiments, it was decided to focus on three elements - Cr at 399.15 nm, Pb at 363.96 nm and 364.73 nm, and V at 370.36 nm. All of these emission lines were of moderate intensity.

#### Experimental

The experimental setup used in the simultaneous multielement analysis study was described in Chapter 3. The spectrometer was set at 364.73 nm which gave a spectral window ranging from 354.73 nm to 374.73 nm. Collected neutral density filters were used in all determinations. In addition, a Q403 filter was placed in front of the spectrometer to block visible light from reaching the detector.

The photodiode array used in the particular phase of the project was the Princeton Instruments ST-110.

### Sample Preparation

The study also required involved sample preparation. Solutions of known concentrations of the three analytes were prepared from stock solutions (Fisher Scientific) with deionized water.

Delivery of the sample volumes onto the microarray cathode surface was accomplished with a calibrated 2  $\mu$ L Eppendorf<sup>®</sup> pipet, which had an accuracy of 0.8% and a precision of 0.2%. Disposable pipet tips were used for all sampling. At the time of this study, the standard pipet was being repaired and recalibrated and was not available for use. All sample volumes for the multicomponent analysis, therefore, were 2  $\mu$ L.

### Experimental Procedure

The experimental procedure used during the phase of the project was similar to that described in Chapter 4, with two exceptions. Firstly, because the sample volumes delivered onto the cathode array was 2  $\mu$ L, a one minute drying step was added to the procedure. Secondly, the spectra generated with the ST 110 photodiode array were all one-dimensional, and so the signal could not be monitored as a function of time. The more sophisticated ST 130 photodiode array was unavailable at the time of this study. The integration times were optimized for this setup.

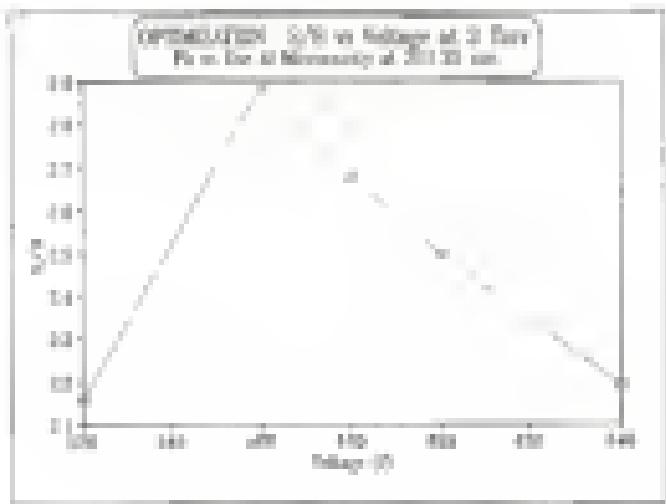
### Optimization

The optimization procedure for the study was much less rigorous than for the single element determination study outlined in Chapter 4. The purpose of this study was to show that simultaneous multielement determination could be achieved with this source, which, under the uncompromised experimental conditions, meant that the best detection limits would not be achieved. Some of the optimizations performed for this phase are presented in Figures 3-1 through 3-6. For Pb, the optimum voltage and pressure were 500 V and 3 Torr, respectively. For Cu, the optimum voltage and pressure were 300 V and 3 Torr. Finally, for V, the optimum voltage and pressure were 500 V and 3 Torr. Having determined the optimum voltage and pressure for the three analytes individually, it was decided that for the simultaneous multielement determination, the compromise voltage and pressure would be set at 500 V and 3 Torr.

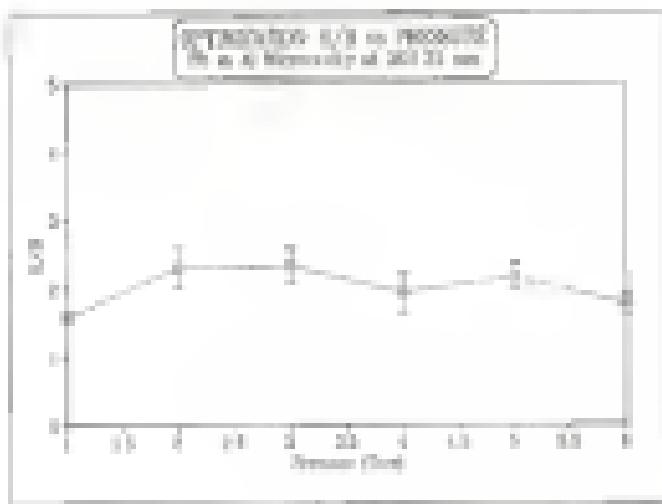
### Results

Figure 3-7 demonstrates that simultaneous multielement detection of discrete mixtures of solution residues of Cr, Pb and V was achieved. Since this work was performed under compromise conditions, using only moderately intense emission lines, determining limits of detection would be of little value. Once it was proved that the stainless steel hollow cathode was amenable to multielement analysis, it could be coupled to a detection system which would allow for the analysis of many (20-60) elements at one time using the most intense

**Figure 5-1** A plot of  $\ln W$  vs. Weights at 0 Torr for  $P_0$  in the Ad mesocamp at 968.39



**Figure 3.3** A plot of 120 ms Pressure for P1 on the left marginality  
at 100 ms.



*Figure 5.3* A plot of  $\Delta\Phi$  vs Voltage for V in the Al macrocycle at 279.38 nm

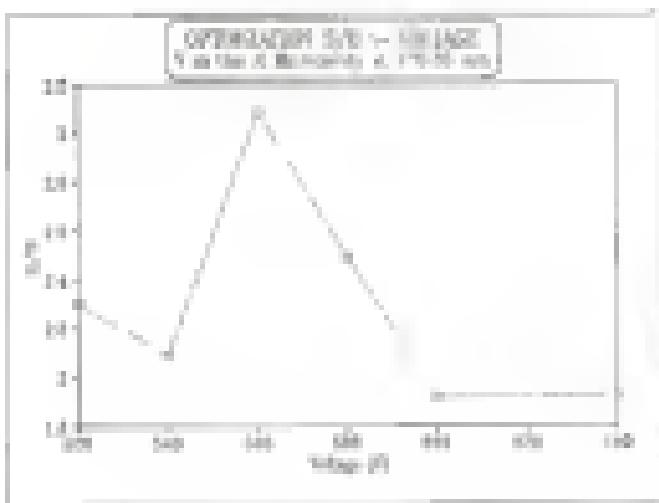


Figure 5-4: A plot of  $\Delta H$  vs Pressure for Y in the Al matrix  
at 120 K.

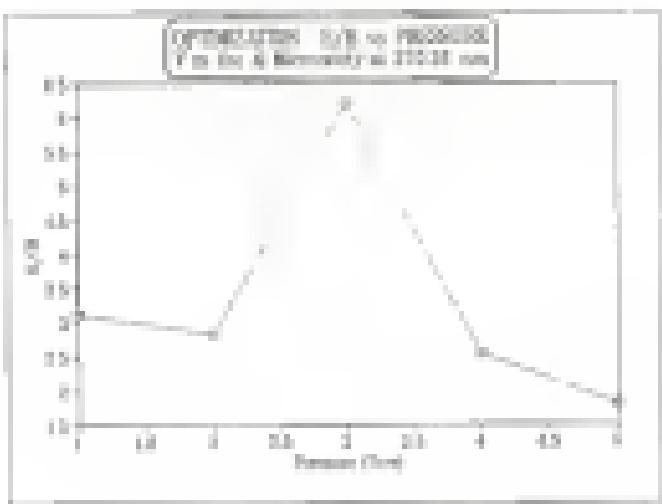
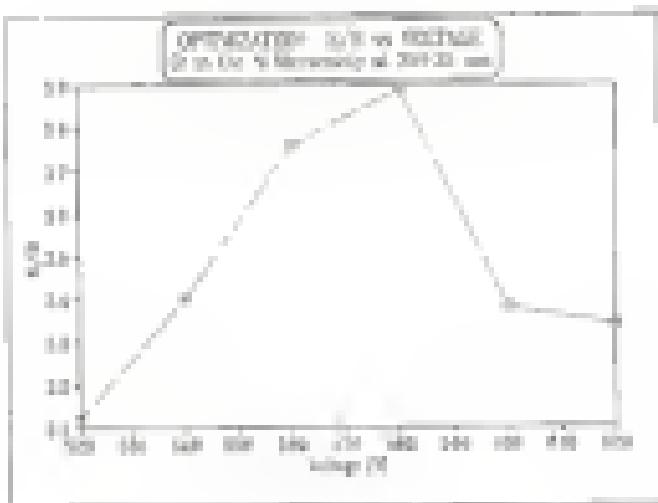


Figure 3-5 A plot of  $S/I$  vs Voltage for Cr as the Al monolayer at 399.71 nm.



**Figure 5-6** A plot of  $\Sigma D$  vs Pressure for Cr in the Al melt casting at 1390 °C.

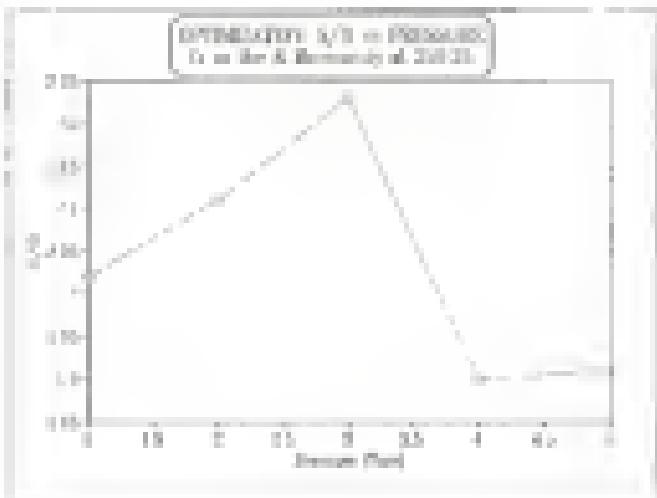
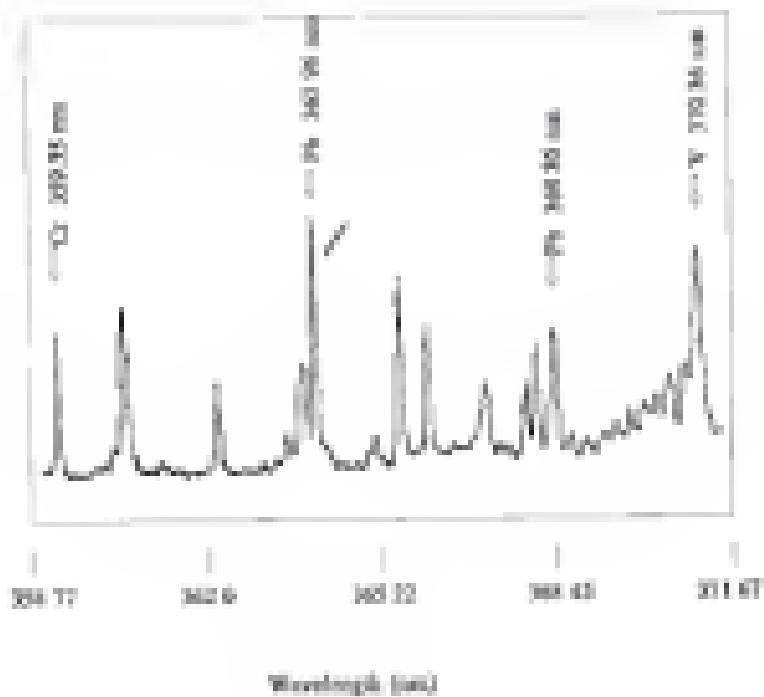


Figure 3.7 A spectrum showing simultaneous multielement determination of Cu, Pb and V

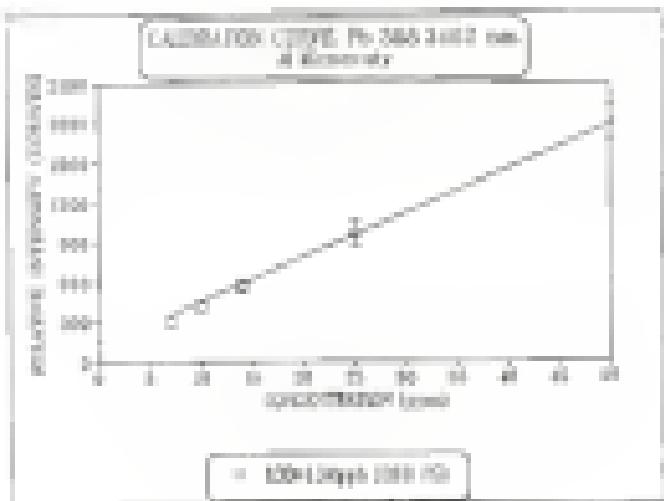


precision limit for each element. Unsurprisingly it was found, it was decided that the detection limit for Pb at this wavelength would be determined and compared to the detection limit presented in the previous chapter for the strongest resonance line. A calibration curve was prepared and is presented in Figure 3-8. The limit of detection based on the  $3\sigma_m$  method was 260 pg. Even though it was over 11000 times higher than the 26-pg detection limit achieved at the 403.77 nm resonance line, it is nevertheless impressive. Amazingly enough, this compares to Beutler<sup>22</sup> glow discharge emission work, in which he reported a detection limit of 100 pg for Pb using a standard hollow cathode and measuring at the very strong 331.3 resonance line.

### Discussion

The findings of this study indicate that the microtoroidal hollow cathode glow discharge shows promise as a sensitive multielement source. Even under unfavorable conditions, the detection limits are excellent. This study, however, was not without its problems. Vanadium proved to be a tricky element to analyze. The discharge with a V sample would sometimes fail to ignite immediately. It was found that in order to obtain a reproducible discharge when V was present, the cathode had to be thoroughly cleaned before each use. Once the vanadium discharge was initiated, however, it was very stable.

Figure S 8. A diffraction image of Pb in the Al microscopy at 248.15 nm.



During this study, alternative discharge gases were tried out, with poor results. Helium gave a very quiet, stable discharge, but its sputtering efficiency was so low, it could not be used for analysis. Neon, on the other hand, allowed for greater sputtering, but presented too many underlying lines in the spectral regions.

## CHAPTER 6 SUMMARY, CONCLUSIONS AND FUTURE WORK

The results presented in Chapters 4 and 5 give evidence to the assertion that the microarc hollow cathode glow discharge emission system is applicable to simultaneous multielement analysis of discrete microsamples and homogeneous of solution residues. When analysing the atomic emission line for each element, it is an excellent source for trace and ultra-trace determination. As a signal burning technique, the microarc is certainly successful.

The limits of detection presented in Chapter 4 were superior to the limits of detection reported from previous glow discharge emission work, as well as many other techniques. The Pb detection limit was especially impressive with a 4-5 order of magnitude improvement over previous glow discharge emission work and a 3-order of magnitude improvement over glow discharge laser excited atomic fluorescence work.

During the course of this project, it was unexpectedly discovered that sample drying time was an important parameter to optimize. This had not previously been discussed in the literature. It was also discovered that complete aging of the cathode resulted in disengaged cathode and was critical for very low detection limits.

Although the work demonstrated that coupling the microconic hollow cathode glow discharge with a photodiode array offered the potential for simultaneous multielement analysis, it could only be observed if the analyte emission lines were within 20 nm of each other. This is a significant drawback to the system presented here. A way to overcome this disadvantage can be suggested. If the current nanochromatograph photodiode array were replaced with a direct reader or a Schottel spectrometer and a CCD detector, 30 or 60 elements could be detected simultaneously using each element's strongest emission line. Since the source has been proven to be so efficient, this system need not be limited by the detector. Such a combination as has just been suggested could prove to be a very powerful multielement technique.

Any future work on this project should focus on improving the precision of the technique. A current controlled power supply would offer a vast improvement in this regard. A more precise sampling technique for samples less than 50 nL could also improve the precision. In addition to these two suggestions, it might be important to design a more efficient cathode cooling system. Improvement in signal output might be accomplished by using a mixture of noble gases for the discharge gas, for example. At He. Signal output could also be improved by coupling the microconic with another signal boosting technique such as a microwave source or an rf source.

In any event, the work has laid a solid foundation for further investigation into a very interesting and promising technique.

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#### BIOGRAPHICAL SKETCH

Cheryl Morgan was born in Massachusetts and raised and educated in New Hampshire. Prior to her chemistry education, she was a public accountant, a business manager and a professional teacher. She received her accounting certificate from the New Hampshire Technical College in 1961. In September of 1966, she went back to college to pursue a degree in chemistry. She received her Bachelor of Science degree from Keene College in Keene, N.H., in May of 1969. She entered the University of Florida's graduate school in the fall of 1969. In 1972, she received her M.S. degree from the University of Florida.

I certify that I have read this study and that, in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy

  
Bruce D. Weisz  
Chair  
Graduate Research Professor of Chemistry

I certify that I have read this study and that in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy

  
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Associate Research Professor of Chemistry

I certify that I have read this study and that in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy

  
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John E. Tyler  
Professor of Chemistry

I certify that I have read this study and that, in my opinion, it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy.



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This dissertation was submitted to the Graduate Faculty of the Department of Chemistry in the College of Liberal Arts and Sciences and to the Graduate School and was accepted as partial fulfillment of the requirements for the degree of Doctor of Philosophy.

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August, 1979

Dean, Graduate School